



Design study of a small long life fast reactor core loaded with Pu without extracting MA

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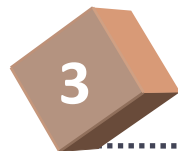
Background

- *Introduction of SMR*
- *Purpose of this work*
- *Calculation tools*



Core performance and results analysis

- *Basic core parameters*
- *Core performance and results analysis*



Summary

1. Background

What is SMR?

- SMR: small and medium sized reactors

innovative SMRs is developed to meet the requirements of some special situations or supplying electricity for a small power grid .

Requirements of long life SMR?

- Long core life up to even more than 10 years;
- Small burnup reactivity loss;

fast reactor is preferred as larger conversion ratio makes small burnup reactivity loss.

- Enhanced non-proliferation capability.

using Pu as nuclear fuel in self-security is desired.

Representatives of long life SMR

- 4S and ENHS reactor

1. Background

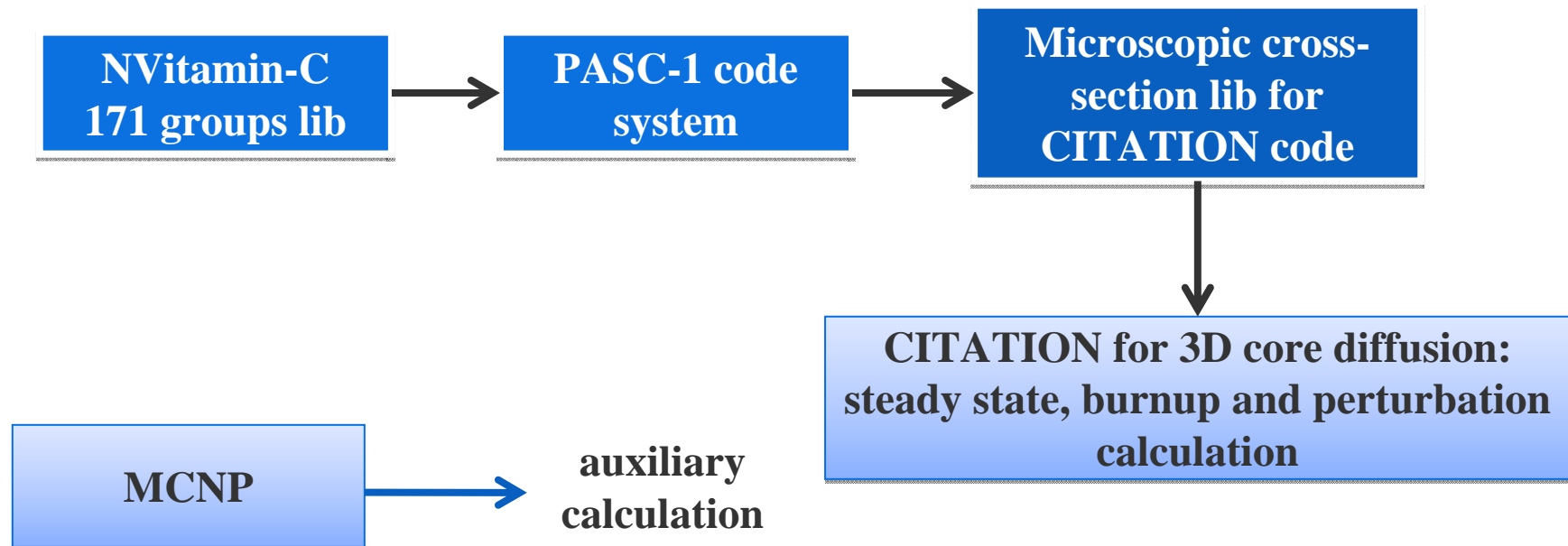
Purpose of the work?

- To demonstrate the feasibility of utilizing *Pu without extracting MA (minor actinides)* as drive fuel for a long life SMR (*non-separation of MA and Pu to enhance fuel non-proliferation*)
 - *Check the impact on core performance of introducing a small amount of MA into fuel*
 - *Compare performance of the core using TRU from PWR with the core using pure Pu as fuel*
 - *Check the enhanced non-proliferation of spent fuel when TRU is utilized as drive fuel*

1. Background

Calculation tools(1/2):

- *N-Vitamin-C 171 groups lib (ENDF/B-VI, JEF-2, CENDL-2 and JENDL-3)*
- *PASC-1 system for few groups cross section processing*
- *CITATION and MCNP*

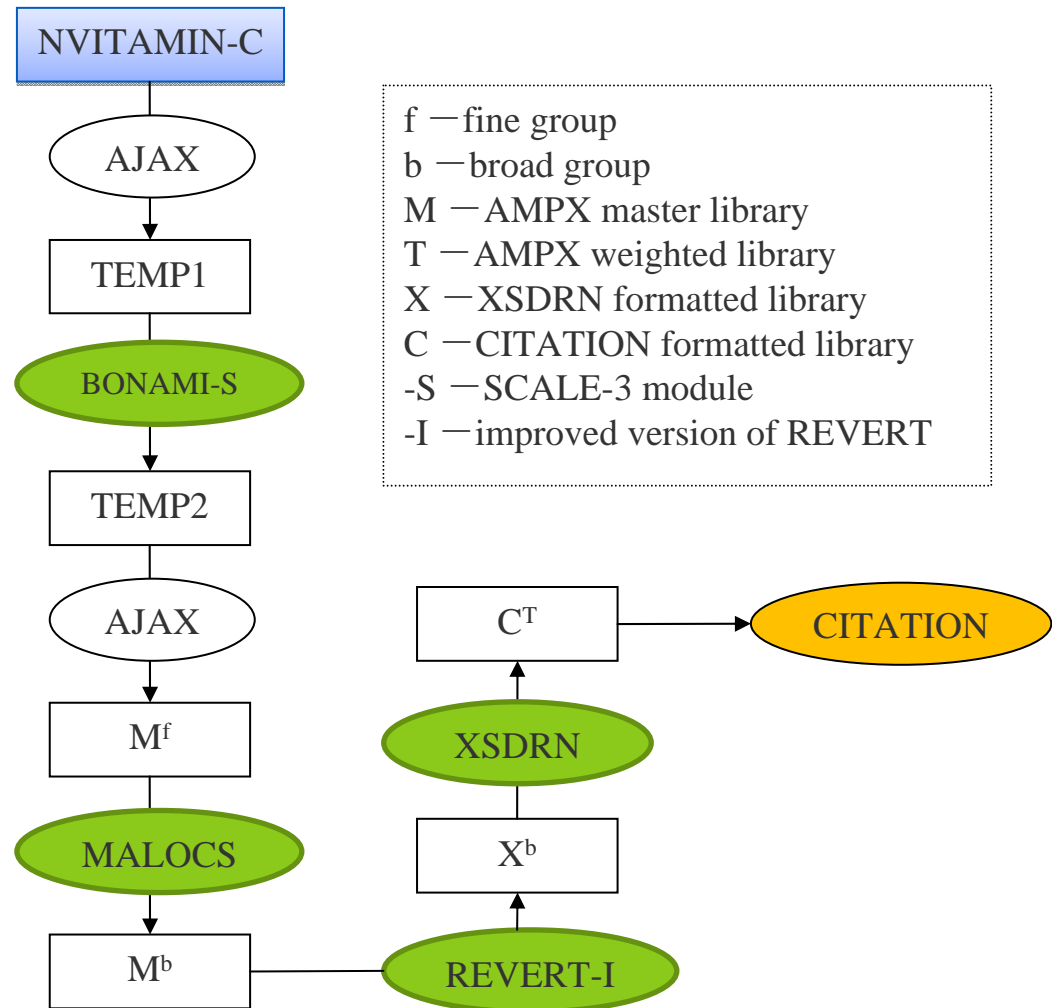


1. Background

Calculation tools(2/2):

– PASC-1 code system: to collapse fine energy group to few group

Flow chart of generation of few groups microscopic cross section lib



2. Core performance and results analysis

Basic core parameters(1/2)

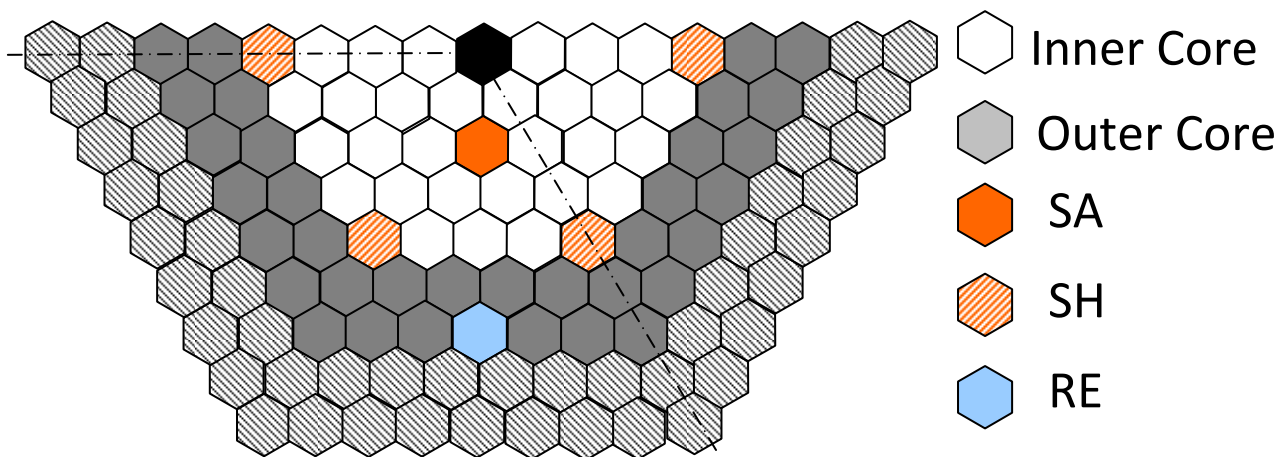
Parameter	Value
Thermal Power/MWt	300
Core dimensions e. q. Dia. × Height	189.181 × 80c
FSA ^a width across flats/cm	16.6 ^m
Characteristics of FSA	
Number of fuel pins per FSA	217
Outer dia. of fuel pins/mm	10.0
P/D	1.1
Cladding thickness/mm	0.6
Fuel smear density	75%T.D.
Gas plenum/fuel volume ratio	1.0
FSA number: Inner/Outer	51/64

^a FSA means fuel sub-assembly.

- *U-Pu-10Zr ternary alloy fuel with smear density 75%TD*
- *300MWt power*
- *Avg. specific power about 22W/gHM*
- *Initial mass loading: U ~11.056t, Pu ~1.79t*

2. Core performance and results analysis

Basic core parameters(2/2)



Radial configuration of core

– 2 enrichment zones

2. Core performance and results analysis

Introduction of different cases in case study

Case	MA amt. wt%	Fuel composition wt%
A	-	10.2Pu-10Zr ^a ; 14.28Pu-10Zr ^b
MA added into fuel		
B	2.5	10.2Pu-2.5MA-10Zr ; 14.28Pu-2.5MA-10Zr
C	5.0	10.2Pu-5.0MA-10Zr ; 14.28Pu-5.0MA-10Zr
D	Non-sep.	10.2Pu-1.249MA-10Zr ; 14.28Pu-1.749MA-10Zr

^a Inner core. Natural uranium is used as supplement in all cases.

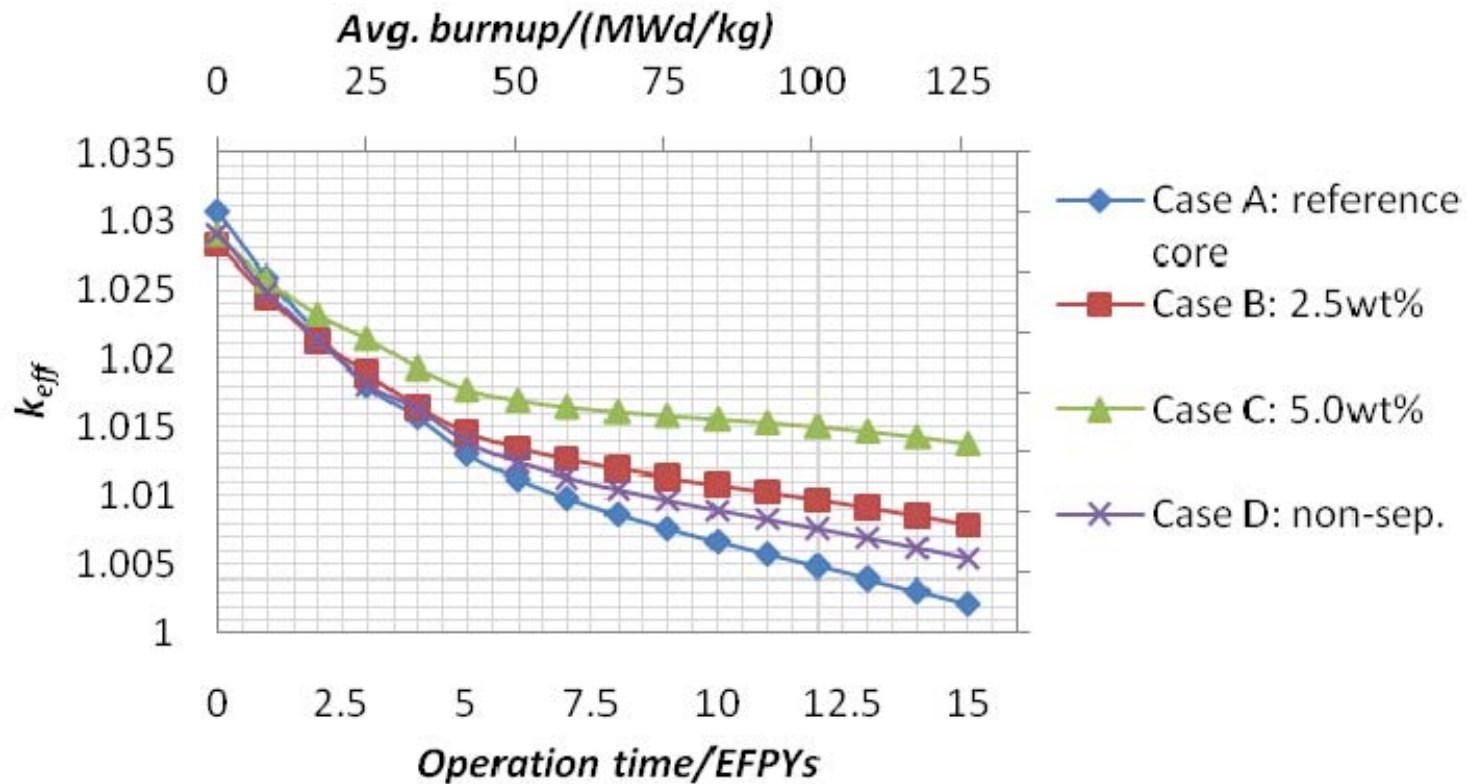
^b Outer core.

– 3 kinds of core:

- case A → pure Pu as fuel, reference core
- case B&C → 2.5 and 5.0wt% MA addition into fuel
- case D → TRU (non-separation of MA and Pu) from PWR as fuel

2. Core performance and results analysis

Burnup reactivity loss(1/2)

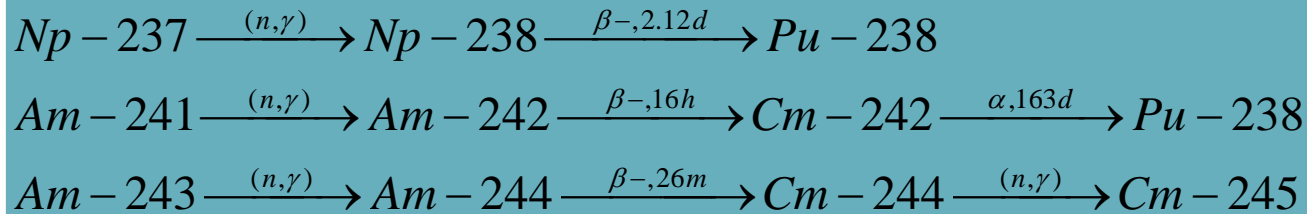


k_{eff} of different cases changes with fuel burnup

2. Core performance and results analysis

Burnup reactivity loss (2/2)

- MA addition reduces $\Delta \rho_{\text{burnup}}$ of core, the more MA the better
- better fission performance of MA capture offspring, like ^{238}Pu



- The core life time is limited to **9~10 EFYs** due to the irradiation damage effect, although from residual reactivity point of view the core can be operated for a longer time.
- assumption of limited neutron fluence is $4 \times 10^{23}/\text{cm}^2$

Only from viewpoint of burnup reactivity swing, MA addition into fuel brings favorable consequence.

2. Core performance and results analysis

Kinetic parameters and reactivity feedback

$$\Delta\rho = K_D \frac{\ln T_2}{\ln T_1}$$

CASE	β_{eff} pcm	Λ $10^{-7}s$	Dop. Effect K_D/pcm	Na void worth ^{*a} \$
A	381.934	3.261	-435.2	3.408
B	359.158	2.821	-340.3	4.747
C	337.680	2.475	-268.4	6.178
D	368.221	2.992	-377.1	4.192

^{*a} Assumption of voiding the whole core and core upper region in uniform is made.

- with MA addition, β_{eff} , Λ and Doppler feedback will decrease, while Na void reactivity will increase
- Compared to β_{eff} , Doppler feedback and Na void reactivity is very sensitive to MA percentage in fuel
- Compared to core with pure Pu fuel, loading TRU (non-separation of MA and Pu) from PWR as a group will bring small impact on core performance
 - mainly because of small MA percentage in TRU from PWR spent fuel

2. Core performance and results analysis

Spent fuel characteristics of different cases(1/2)

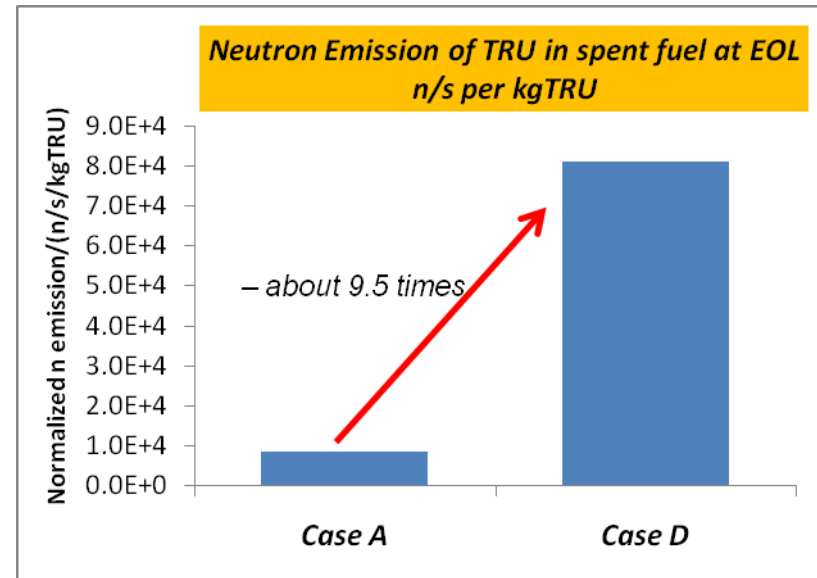
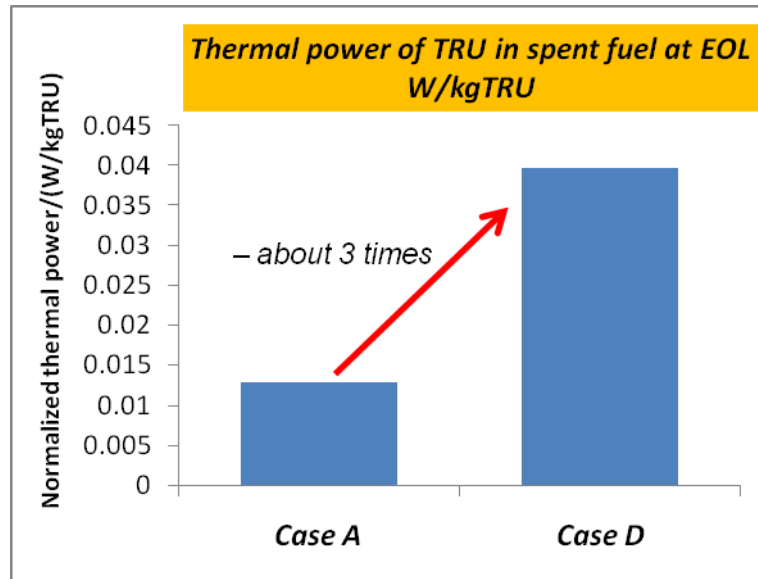
BOL and EOL TRU composition of CASE A and D

Mass/kg	Case A		Case D	
	<i>(Pure Pu as drive fuel)</i>		<i>(Whole TRU as drive fuel)</i>	
	<i>BOL</i>	<i>EOL</i>	<i>BOL</i>	<i>EOL</i>
Pu	1790	1697	1790	1706
MA	0	43	219	185
MA/TRU	0	2.471%	10.901%	9.783%

- *proliferation resistance of BOL initial loading fuel and EOL discharged fuel are both increased when TRU from PWR used as drive fuel*
 - *because high MA percentage in BOL fuel and EOL spent fuel*
- *additional benefit of loading TRU from PWR as a group is that considerable amount of MA is “burned”, while in the reference core, MA inventory increases with the fuel burnup*

2. Core performance and results analysis

Spent fuel characteristics of different cases(2/2)



- *thermal power* and, especially, *neutron emission rate* of TRU in spent fuel at BOL are both increased, which means enhanced non-proliferation capacity

3. Summary

- The work focused on design study of loading TRU from PWR as a group in a small long life SMR
 - Along with MA addition into fuel, advantages including:
 - *reduced burnup reactivity swing;*
 - *transmutation of considerable amount of MA;*
 - *enhanced proliferation resistance*
- while disadvantages are penalties on:**
- *kinetic parameters;*
 - *reactivity feedback performance (like Doppler feedback and Na void worth);*
- Compared to the core with pure Pu as drive fuel, loading TRU from PWR without separation of MA and Pu will introduce **small** impact on core performance, while the benefit of significantly enhanced proliferation resistance can be obtained



Thanks for your attention.