

**Numerical Analysis of Flow and Heat Transfer
in a Fuel Subassembly of SFRs with Porous Model**

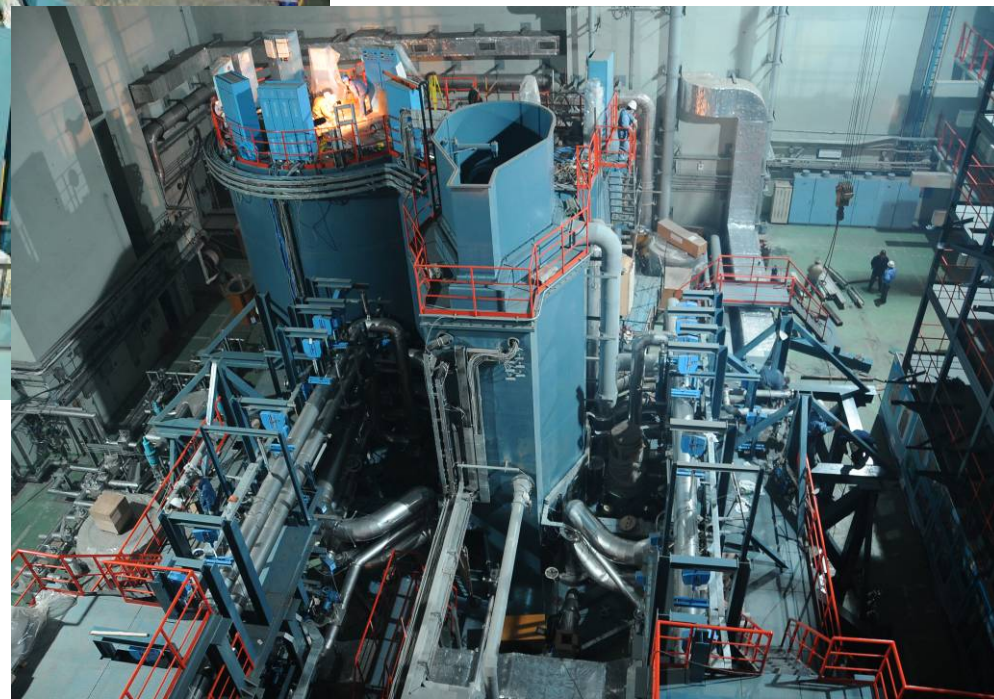
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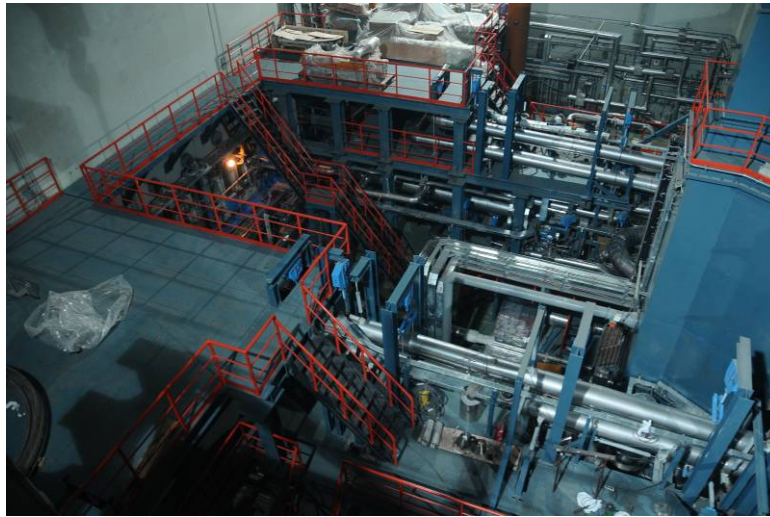
Current status of the CEFR



Reactor Hall



China Institute of Atomic Energy



Piping line of secondary circuit

Main control room



I&C system room



Milestones

- ✓ **1995.12.09, project approved;**
- ✓ **1997.11.13, primary design approved;**
- ✓ **2000.05.30, first pot concrete;**
- ✓ **2004.11.30, detail design finished;**
- ✓ **2009.05.30, start primary circuit commissioning.**

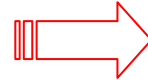
Numerical Analysis of Flow and Heat Transfer in a Fuel Subassembly of SFRs with Porous Model

- N-S formula and porous model
- Pressure drop model and heat transfer model
- Numerical simulation results

System analysis code

More accurate
More detailed

One dimensional



Three dimensional

OASIS



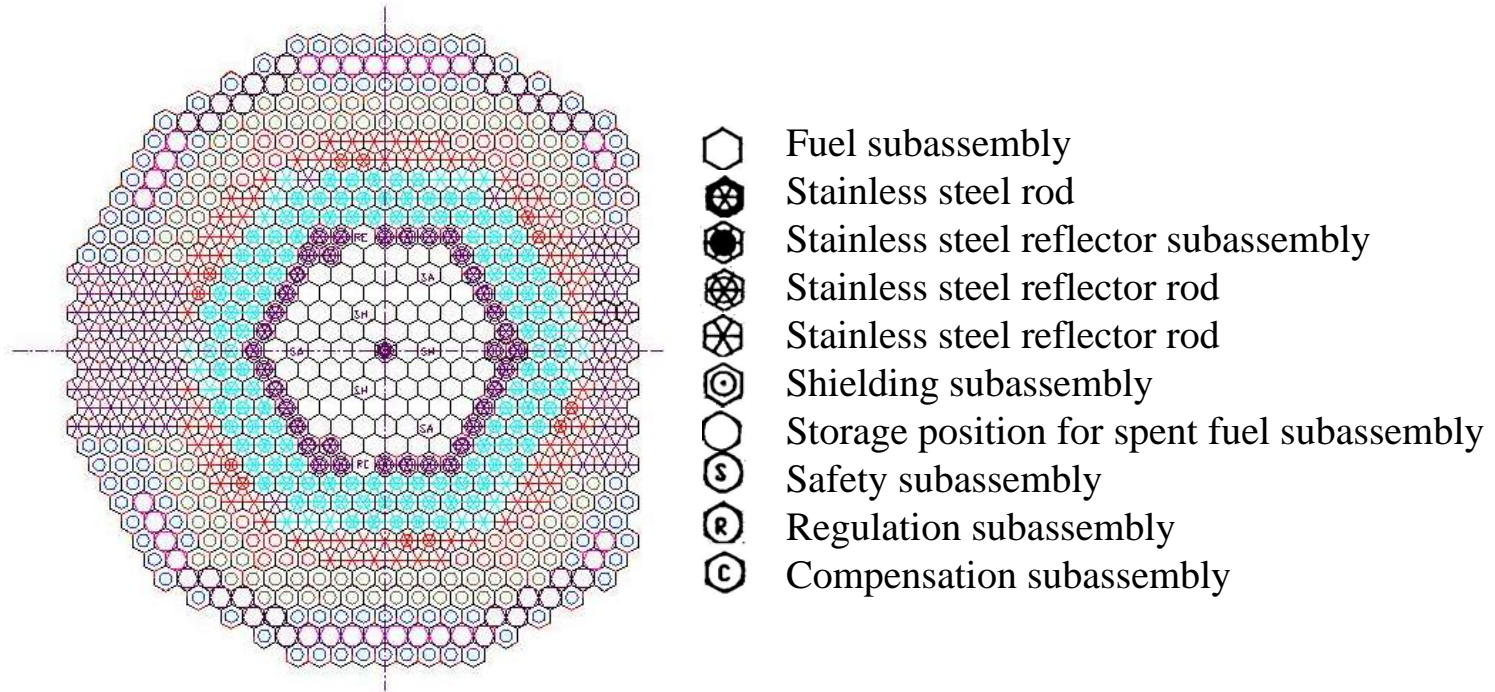
SASSYS

CFD method

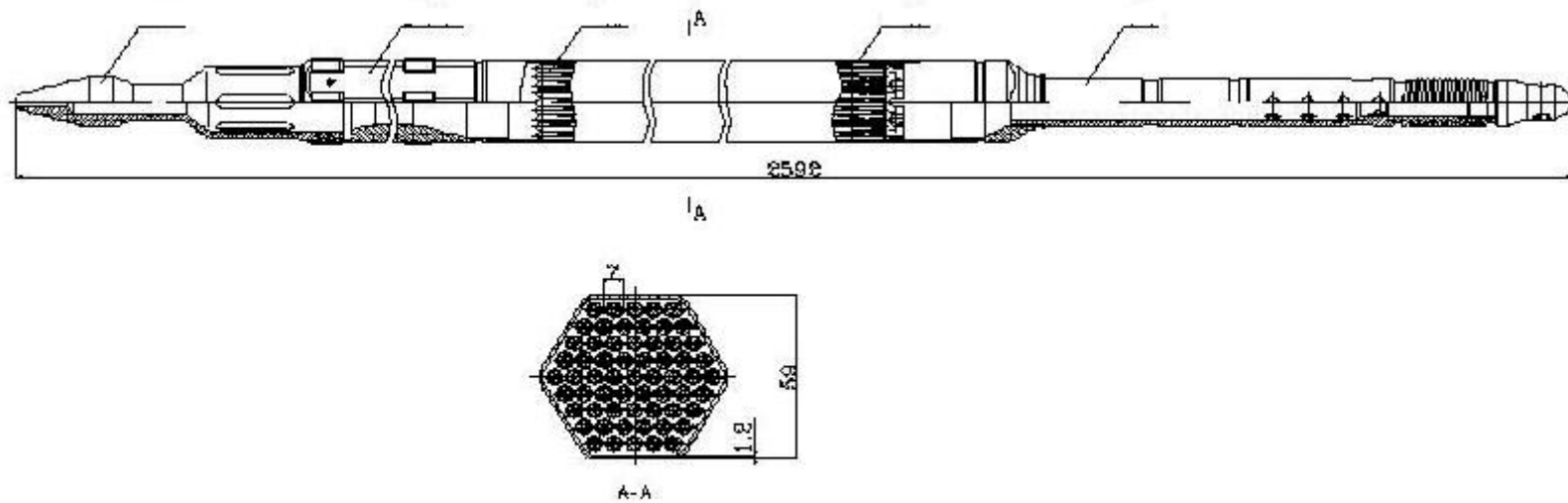
Relap



Experimental data



CEFR Core Configuration



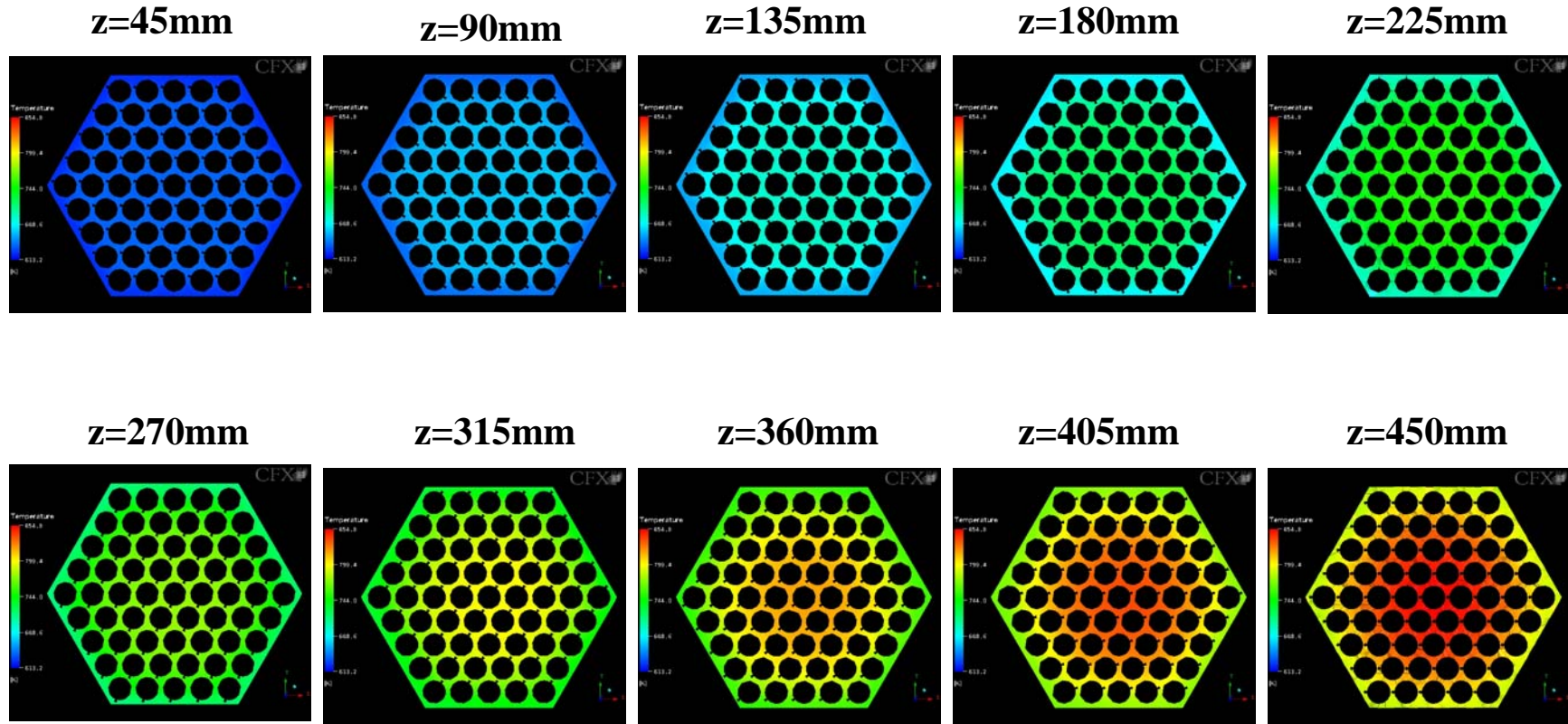
Layout of Fuel Subassembly



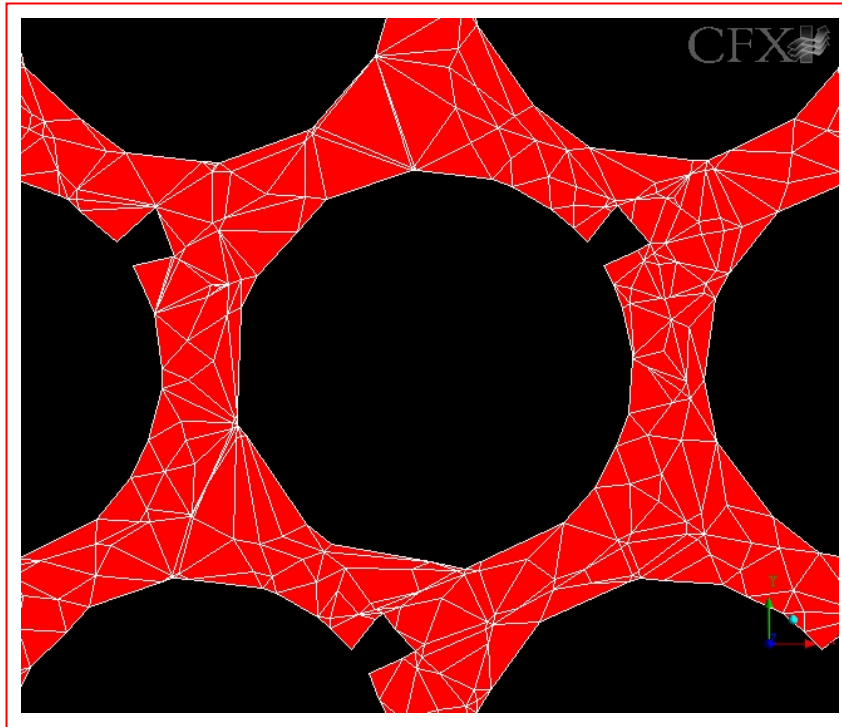
P-Pitch
D-Pin Diameter
s-Wire Diameter
H-Lead
L-Pin Length

Rod Bundle

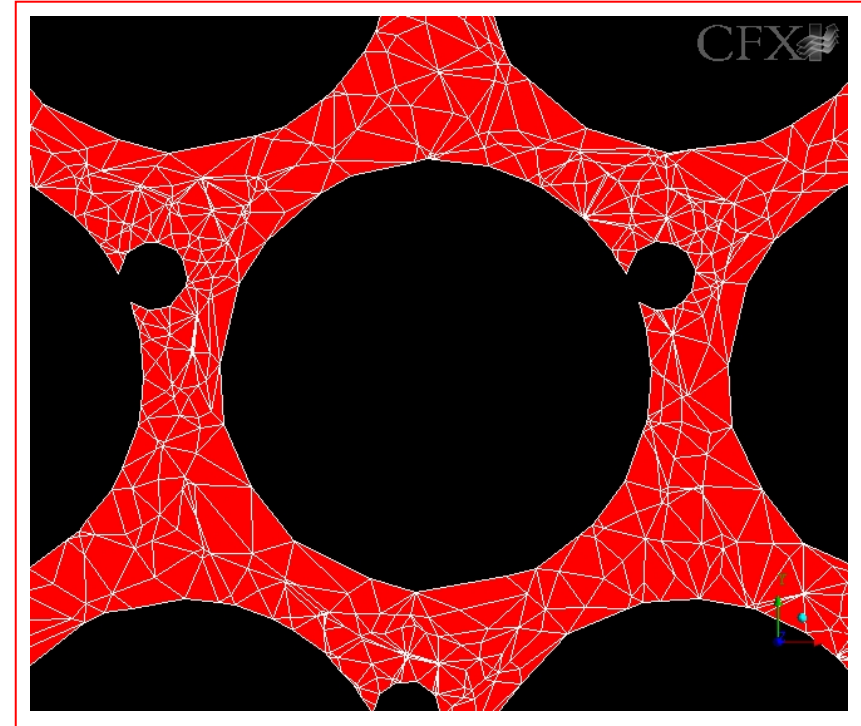
Rod wrapped by helical wire



Temperature Distribution at 10 Cross Sections

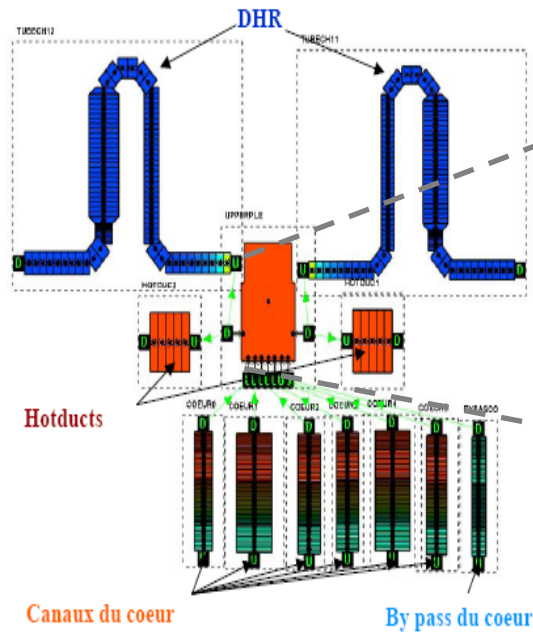


2.4 million meshes
1 CPU, 3 hours



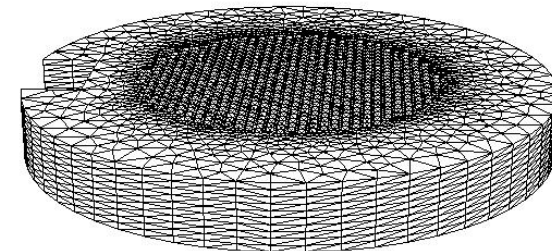
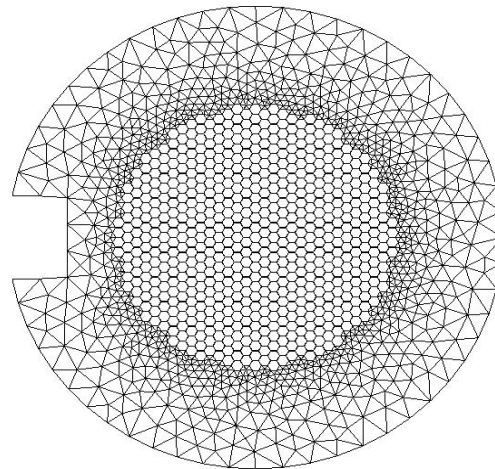
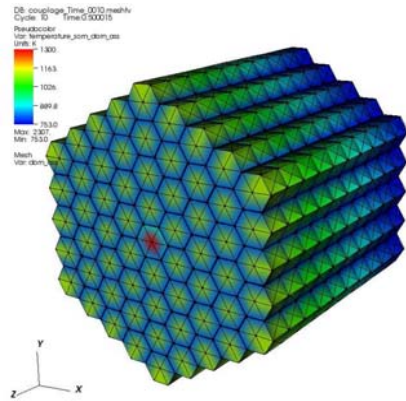
20 million meshes
10CPU, Several days
Better

Comparison of Mesh Quality

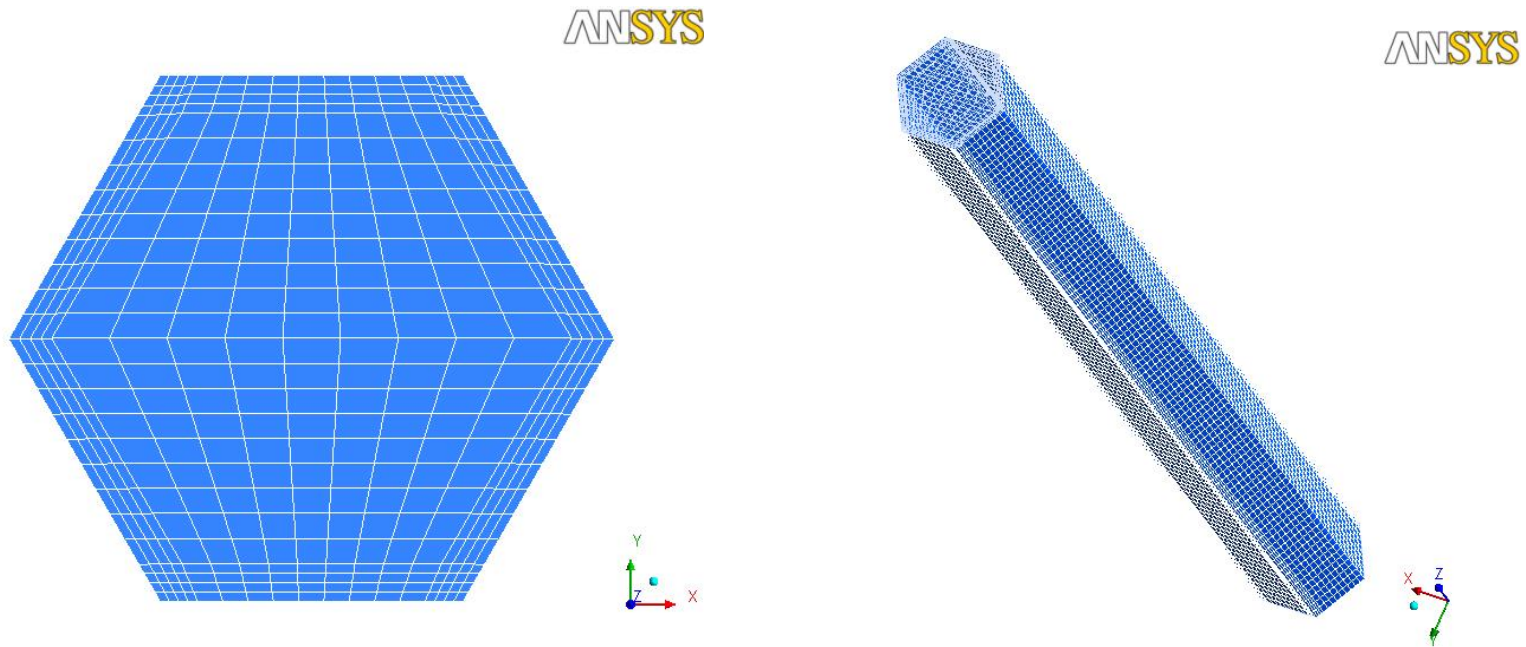


CATHARE-ML

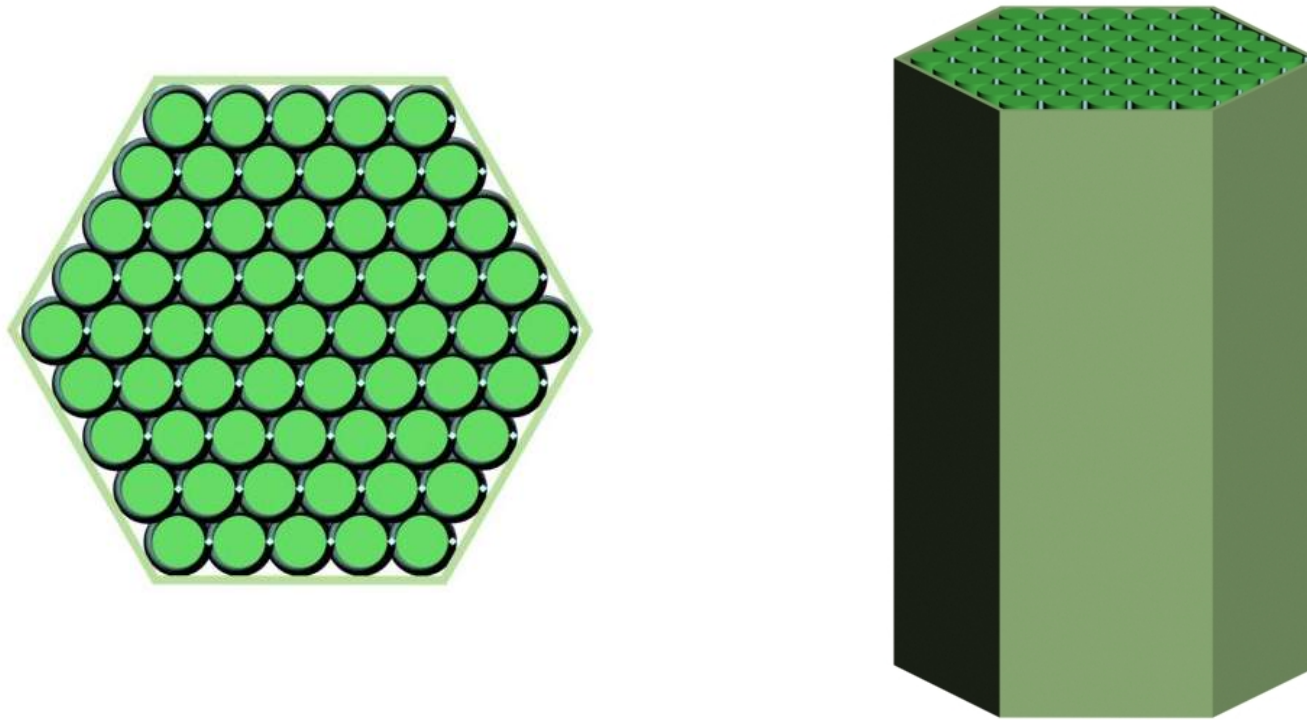
New system code program in France



Porous model consideration



Meshes of the SA active part



Volume porosity and surface porosity

Governing Equations in Code

Darcy's law

$$-\frac{\partial p}{\partial x_i} = \frac{\mu}{K_{perm}} U_i + K_{loss} \frac{\rho}{2} |U| U_i$$

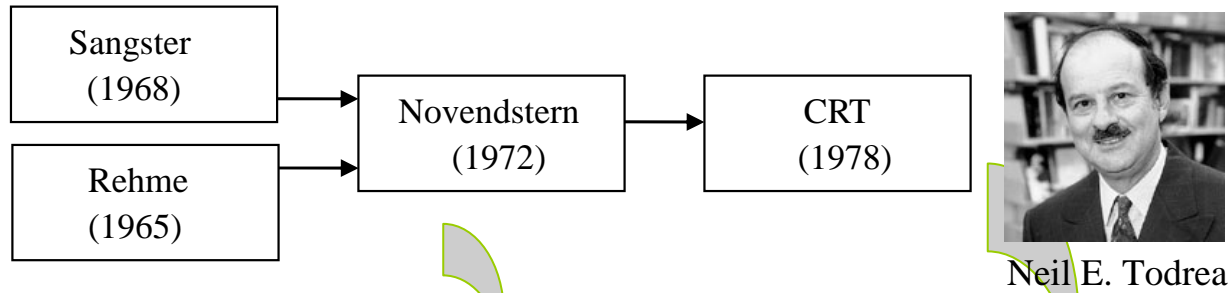
Advection-diffusion equation

$$\frac{\partial}{\partial t} (\gamma \rho \Phi) + \nabla \cdot (\rho K \cdot U \Phi) - \nabla \cdot (\Gamma K \cdot \nabla \Phi) = \gamma S$$

Equations for conservation of mass and momentum

$$\frac{\partial}{\partial t} \gamma \rho + \nabla \cdot (\rho K \cdot U) = 0$$

Pressure Drop In Rod Bundle



$$\Delta p = Mf_{\text{光滑}} \frac{L}{D_{e1}} \frac{\rho V_1^2}{2}$$

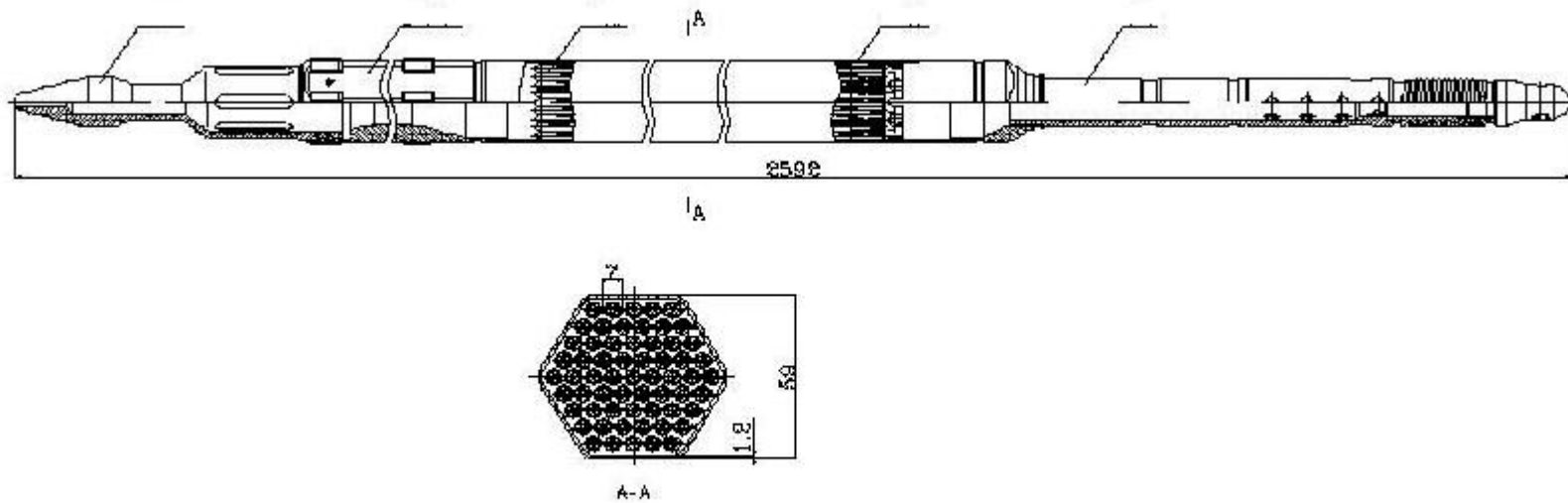
$$\Delta p_1 = f_{s1} \frac{L}{D_{e1}} \frac{\rho V_1^2}{2} \left[1 + C_1 \frac{A_{r1}}{A_1} \frac{D_{e1}}{H} \frac{P^2}{(\pi P)^2 + H^2} \right]$$

$$\Delta p_2 = f_{s2} \frac{L}{D_{e2}} \frac{\rho V_2^2}{2} \left\{ 1 + \left[C_2 n \left(\frac{V_T}{V_2} \right)_{\text{间隙}} \right]^2 \right\}^{1.375}$$

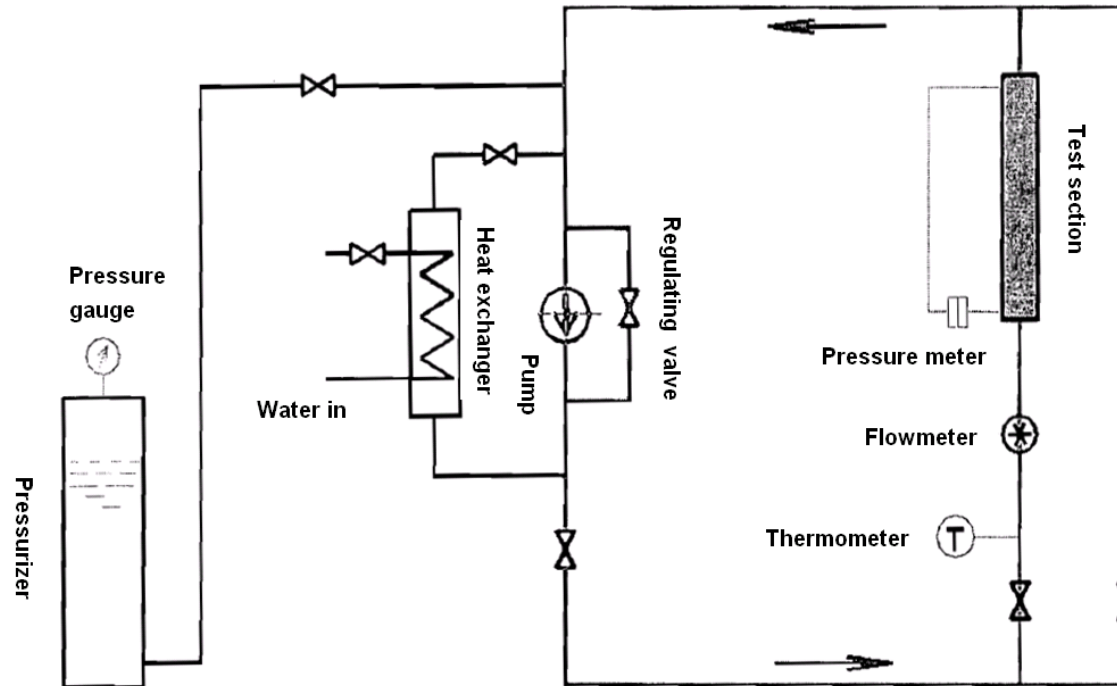
$$\Delta p = \frac{N_1 A_1}{N_1 A_1 + N_2 A_2} \Delta p_1 + \frac{N_2 A_2}{N_1 A_1 + N_2 A_2} \Delta p_2$$

Colebrook Formula:

$$\frac{1}{f^{0.5}} = -4 \lg \left[\frac{(\varepsilon / D)}{3.7} + \frac{1.255}{(R_e f^{0.5})} \right]$$



Layout of Test Subassembly

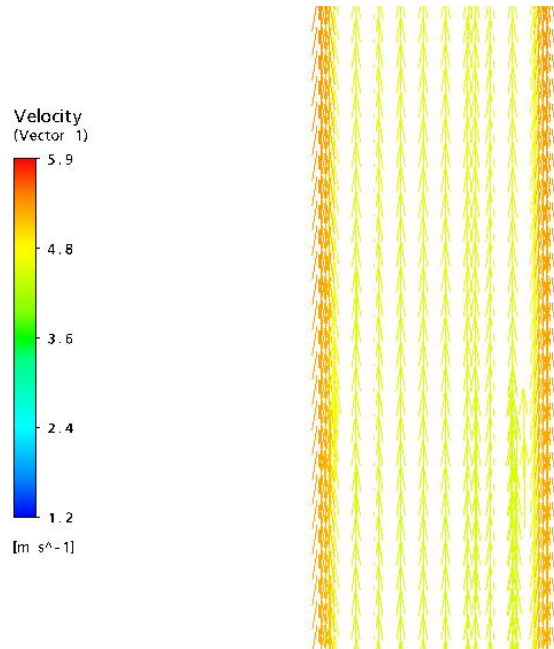


Test rig for pressure drop of SA

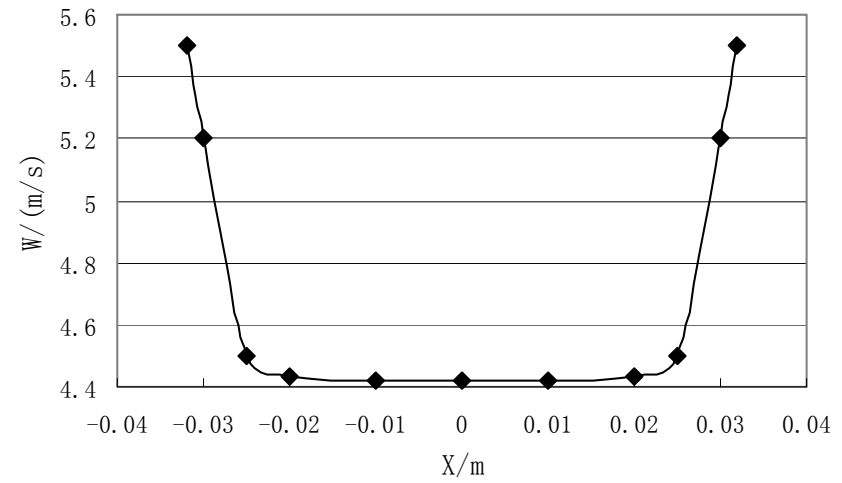
Heat transfer model

$$\frac{\partial}{\partial t}(\gamma\rho H) + \nabla \cdot (\rho K \cdot UH) - \nabla \cdot ((\rho C_p \varepsilon + \Gamma_e K) \cdot \nabla H) = \gamma S^H$$

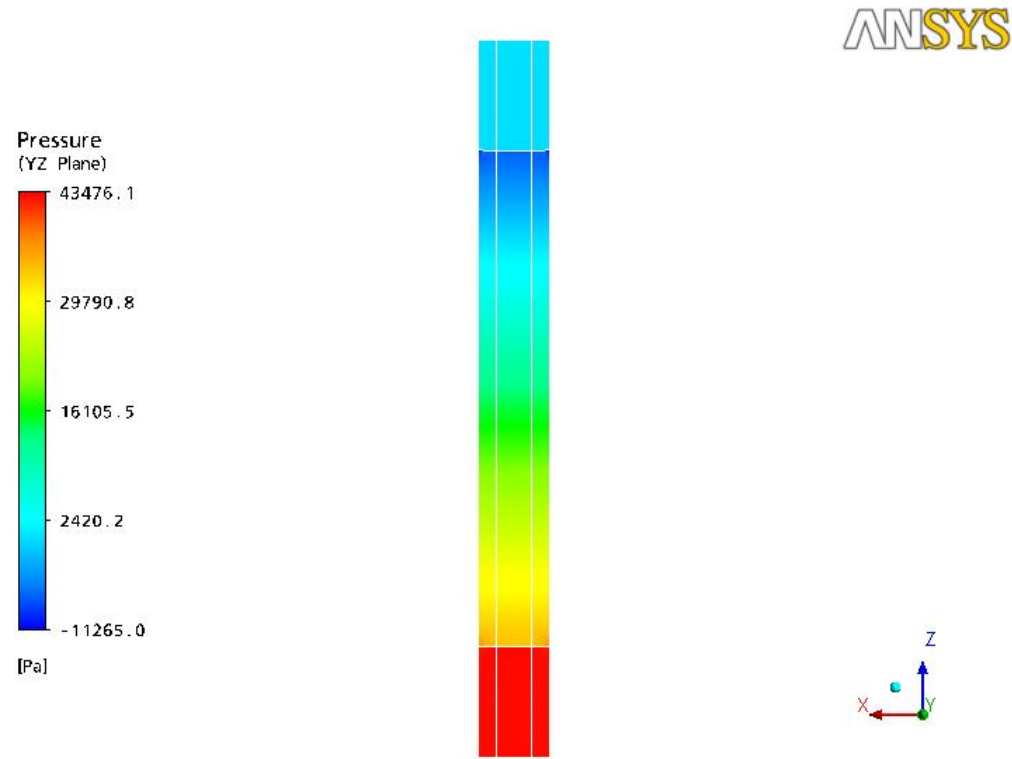
$$\varepsilon = \left(\frac{D}{H}\right) \left[0.85 - 12.8 \left(\left| \frac{P}{D} - 1.25 \right| \right)^{1.424} \right] \frac{\bar{\lambda}_a}{\lambda_{LI}}$$



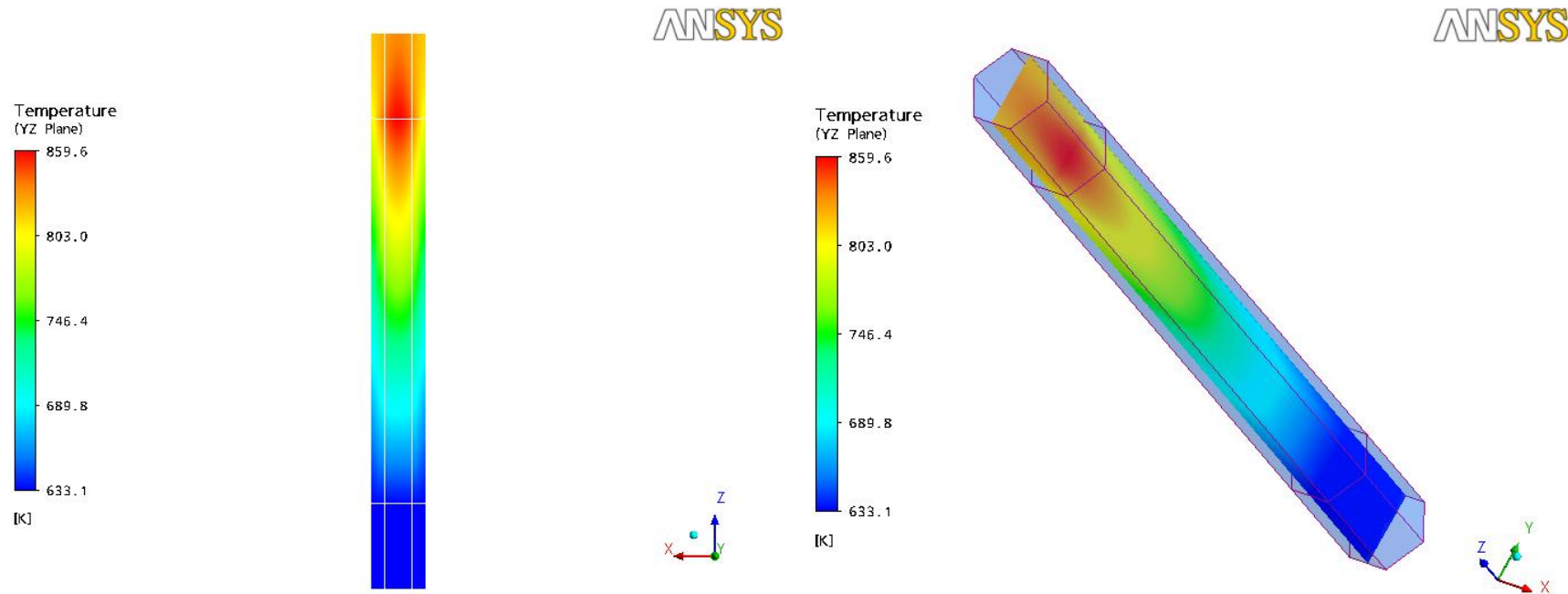
ANSYS



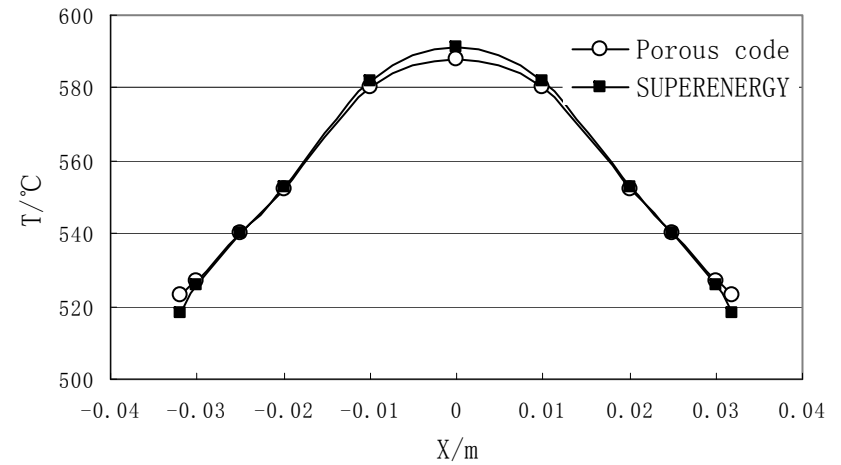
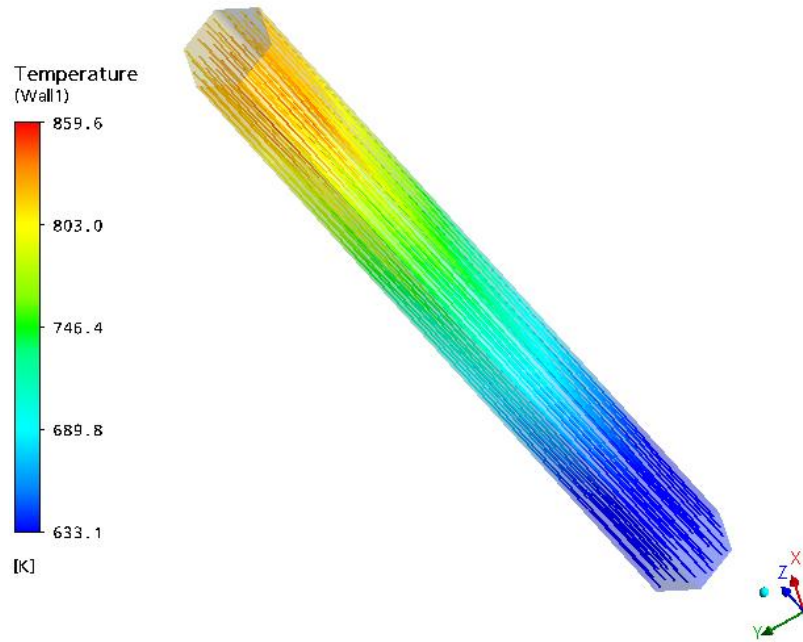
Axial velocity distribution



Pressure drop in the active part

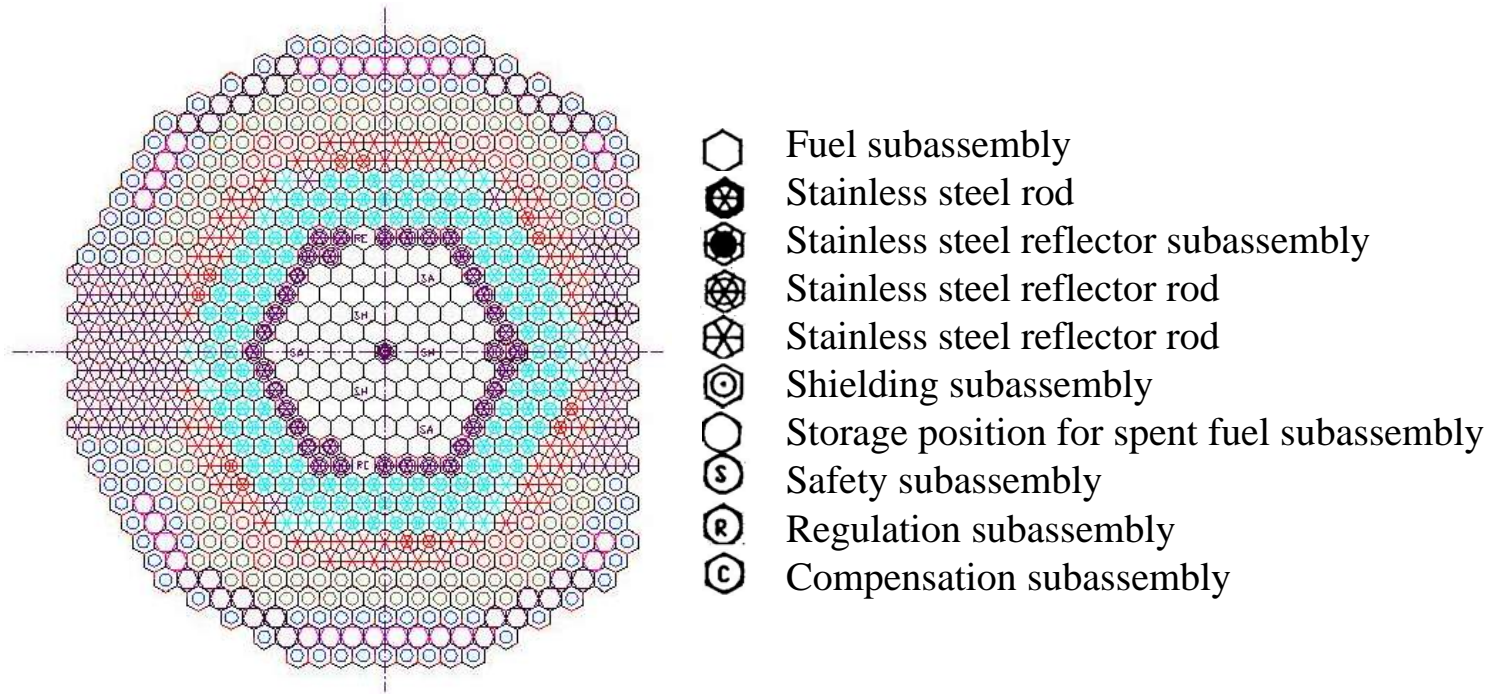


Axial temperature distribution

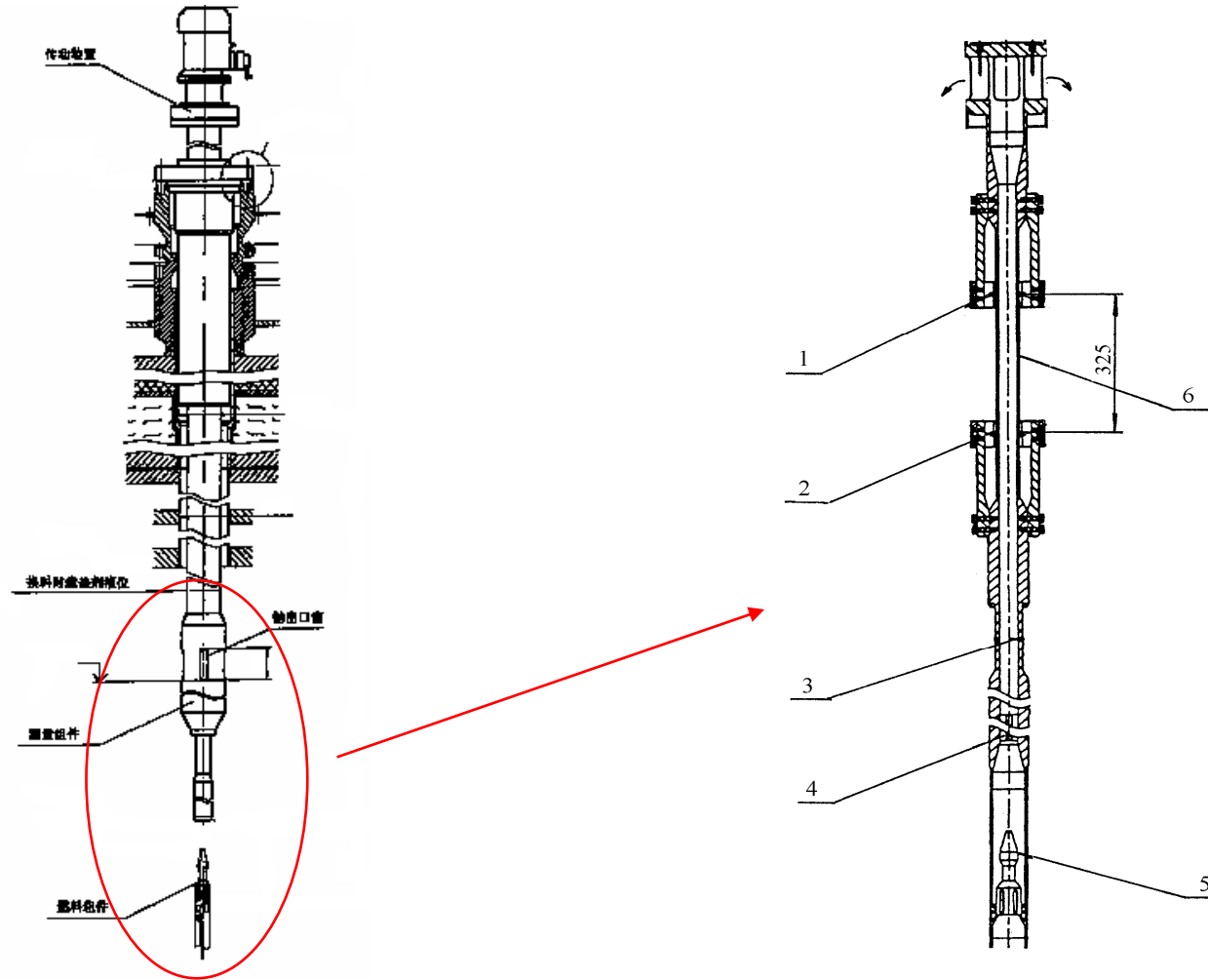


Axial temperature distribution

Whole core flowrate distribution test in CEFR



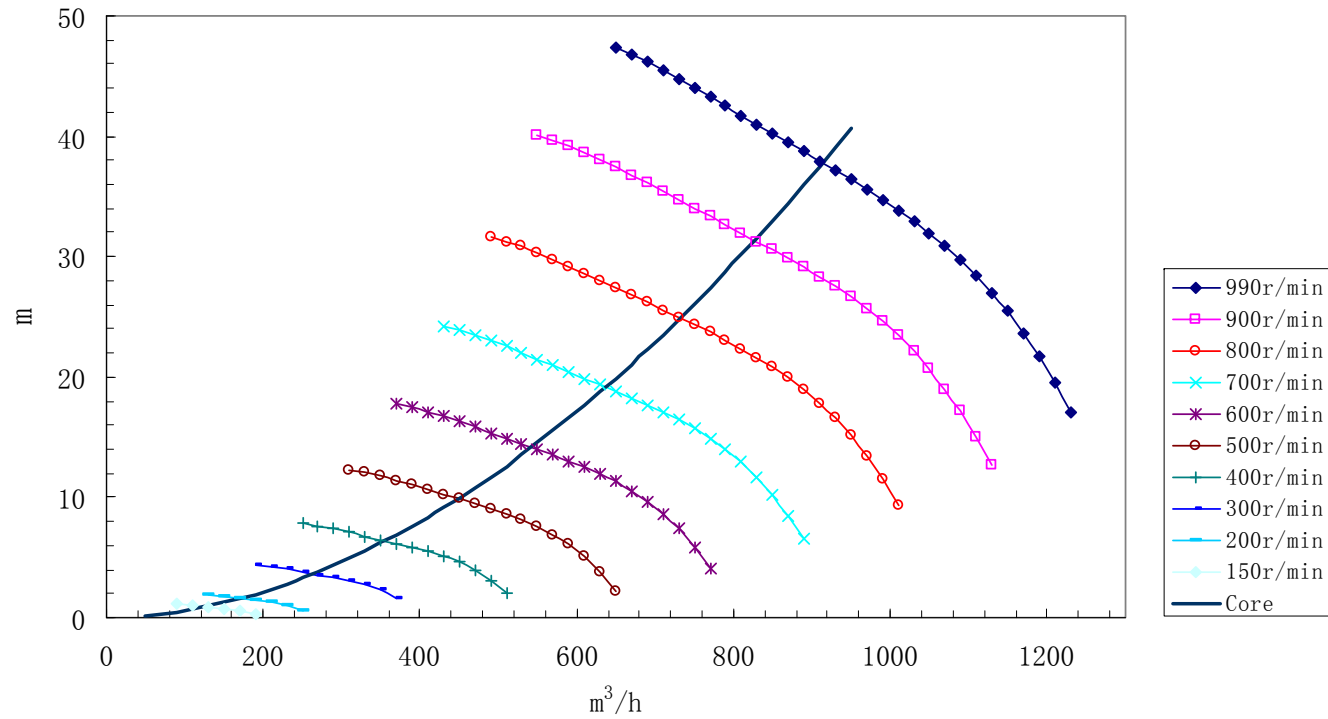
CEFR Core Configuration



Permanent-magnet sodium flowmeter



Reactor block model

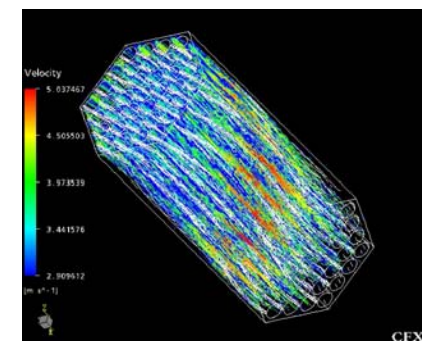
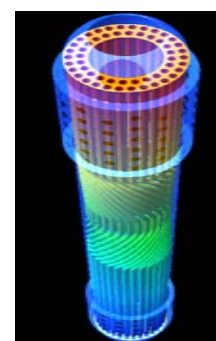
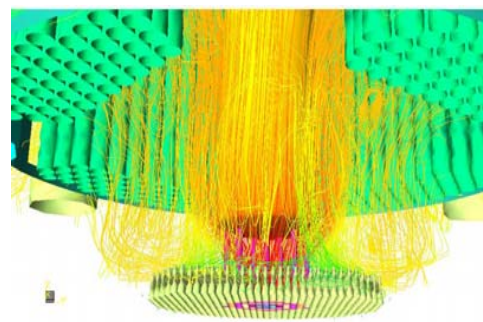
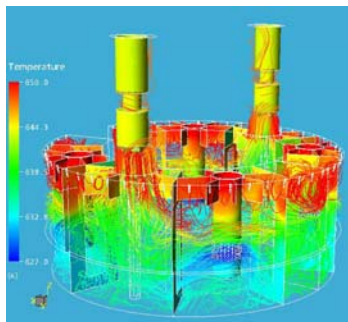
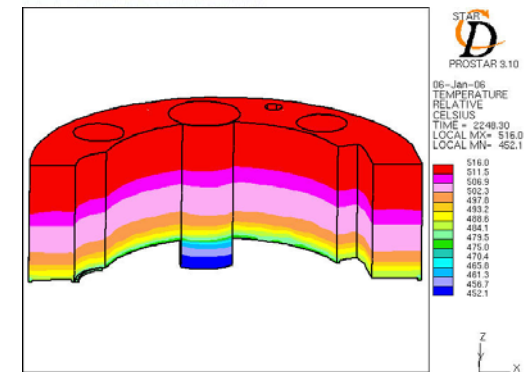
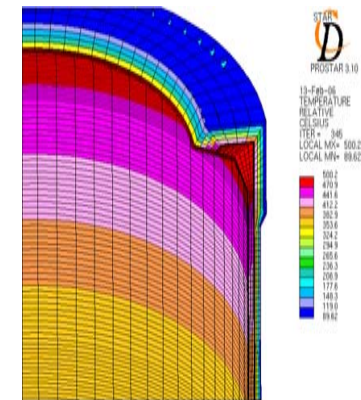


Hydraulic characteristics of the core

Issues requiring further research and development:

- Flowrate distribution results.
- Experimental database for DHRS.
- Thermal-hydraulics coupling with physics.

New system code to optimize design and guide reactor operation.



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CEFR

- Thank you!