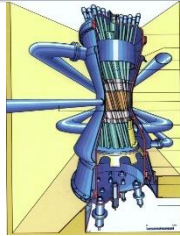


Feasibility Studies for Simultaneous Irradiation of NBSR & MITR Fuel Elements in the BR2 Reactor

S. Kalcheva, S. Van Dyck, S. Van den Berghe, G. Van den Branden

IGORR 18th: International Group on Research Reactors,
Sydney, Australia, December 3-7, 2017



Feasibility Studies for Simultaneous Irradiation of NBSR & MITR Fuel Elements in the BR2 Reactor

Steven Van Dyck
Manager of BR2 Reactor

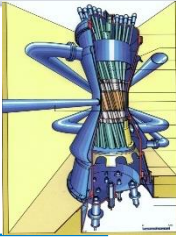
Sven Van den Berghe
BR2 Reactor Stakeholder

Geert Van den Branden
Head of Reactor Control & Experiments

Silva Kalcheva
Reactor Core Load Manager

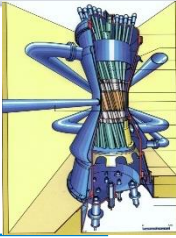
Nuclear Materials Science Institute
SCK•CEN, BR2 Reactor, 2400 Mol – Belgium

Outline

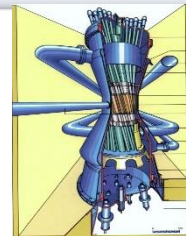


- Introduction
- Purpose of Design Demonstration Element tests
- Technical requirements for DDE
- MCNP calculation methodology
 - Full core 3-D MCNP modeling of BR2 reactor
 - 3-D modelling of DDE-MITR and DDE-NBSR
 - 3-D power and burn-up evolution simulation
- Calculation results
- Summary

Introduction

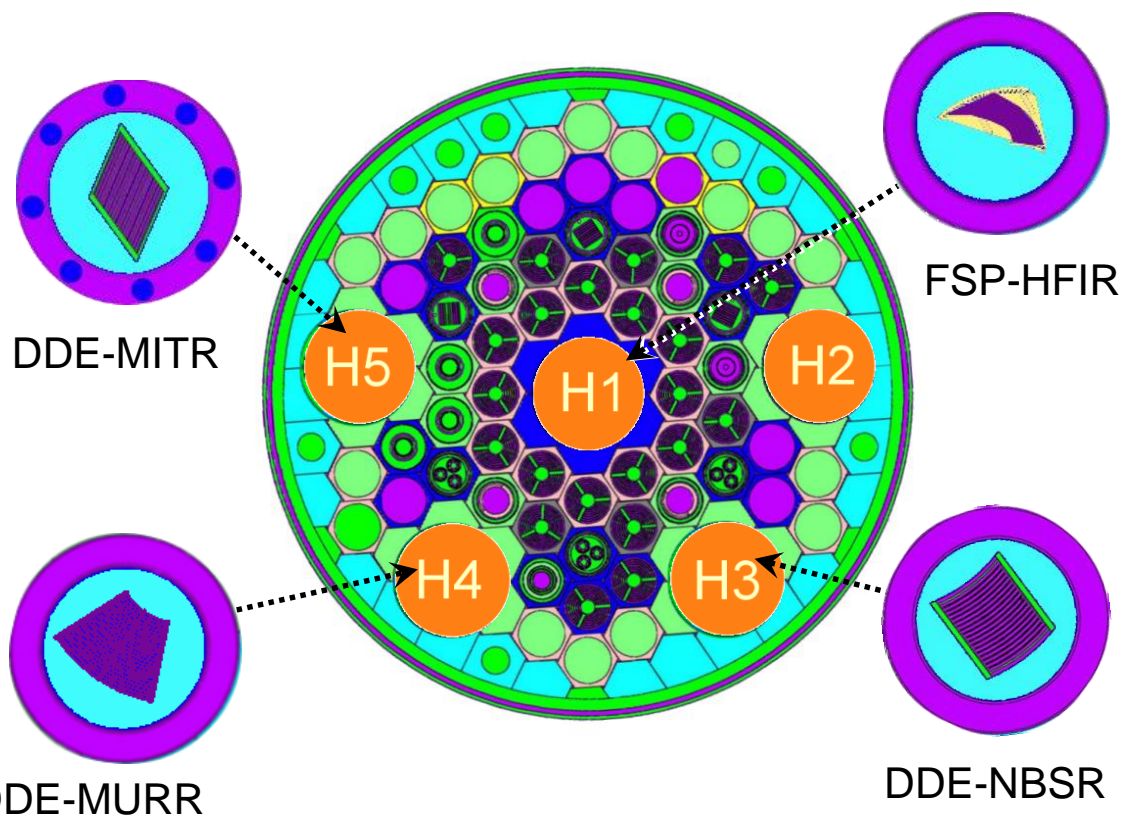


- Four Design Demonstration Element (DDE) tests foreseen in the US High Performance Research Reactor (USHPRR) conversion program:
 - Missouri University Research Reactor (MURR),
 - Massachusetts Institute of Technology Reactor (MITR),
 - National Bureau of Standards Reactor (NBSR) and
 - High Flux Isotope Reactor (HFIR)
- BR2 Reactor along with other MTR (ATR) involved in preliminary feasibility studies



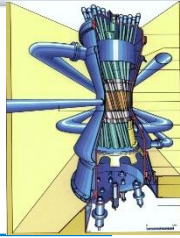
Purpose of DDE tests

- Qualification of the new LEU fuel for each DDE in the BR2 reactor at *conditions that are similar for reactor of origin*



❖ Present study:
scenarios for
*simultaneous
irradiation of
MITR and NBSR
Test Assemblies*

Technical requirements for DDE tests



- Simultaneous irradiation → challenge for core management

- DDE-MITR

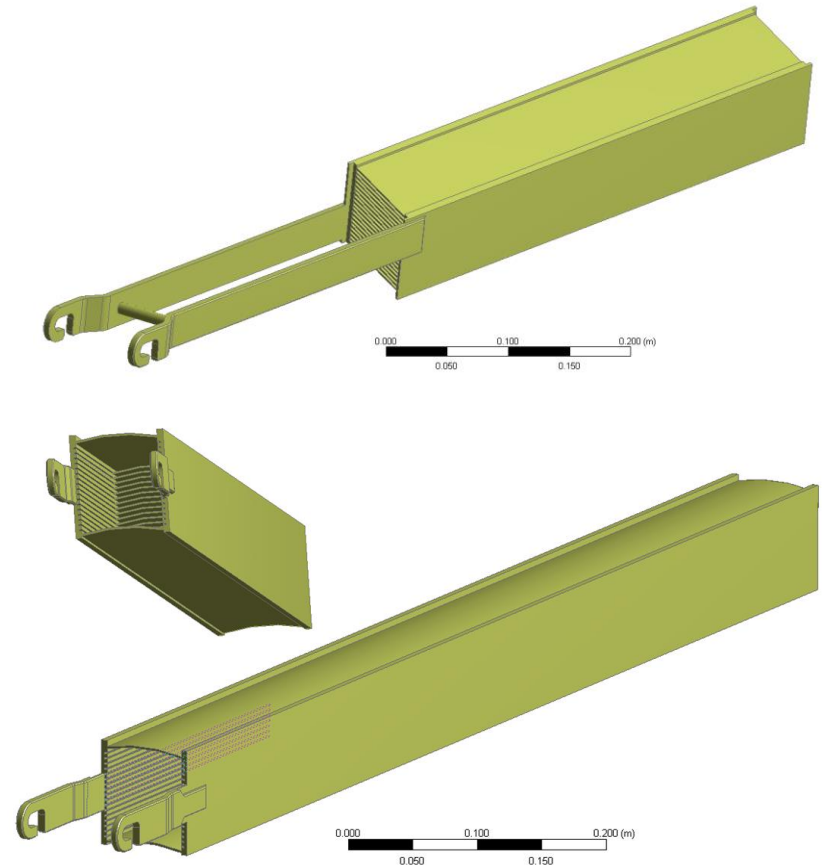
- Q_{\max} (BOL) = **64** W/cm²

- F_{\max} (EOL) = 5.8E21 fiss/cm³

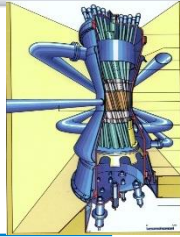
- DDE-NBSR

- Q_{\max} (BOL) = **160** W/cm²

- F_{\max} (EOL) = 7.9E21 fiss/cm³

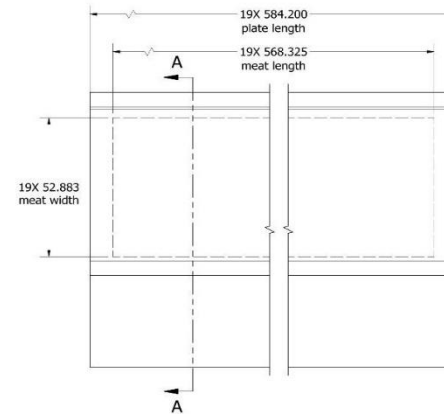
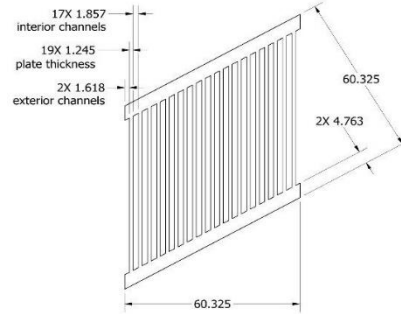


Geometry & dimensions of DDE's

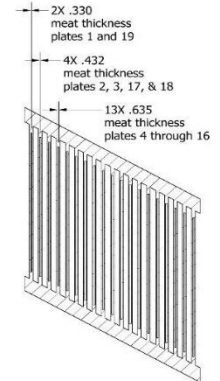


● DDE-MITR

- ❖ rhomboid form
- ❖ 19 plates
- ❖ variable meat thickness



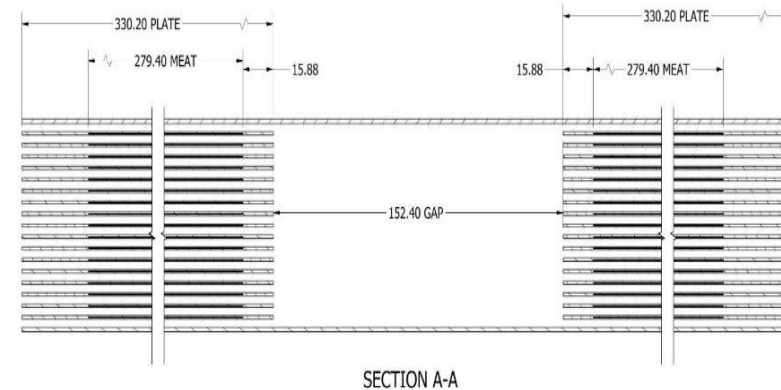
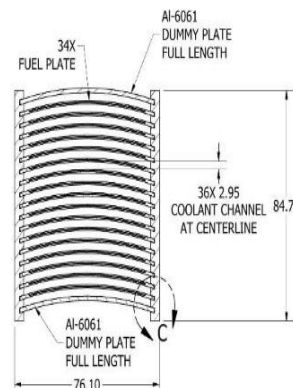
Dimensions in mm



SECTION A-A
SCALE 1

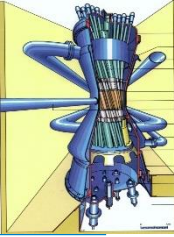
● DDE-NBSR

- ❖ Upper and lower sections
- ❖ Divided by water gap
- ❖ Total 2 x 17 = 34 plates

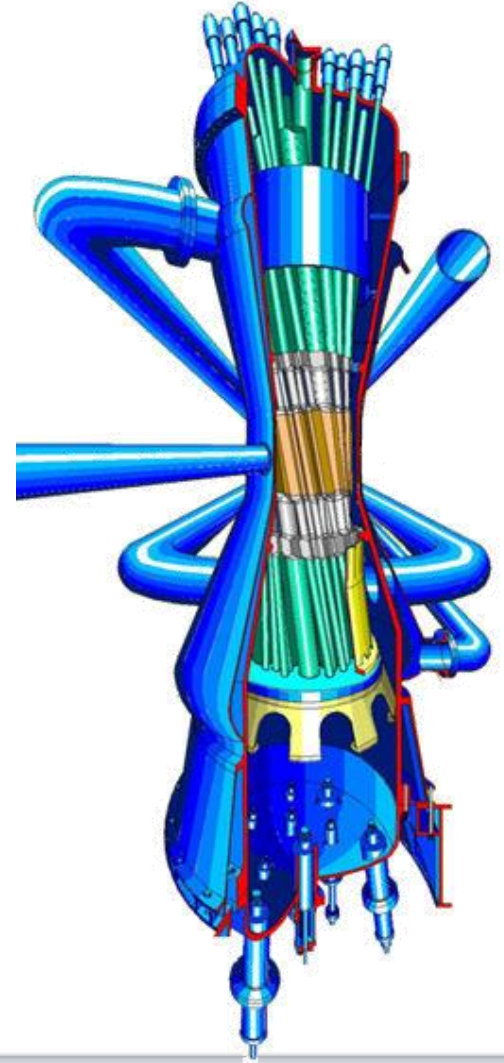


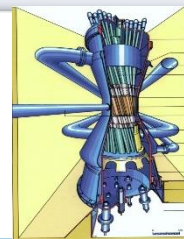
SECTION A-A

Description of BR2 reactor characteristics



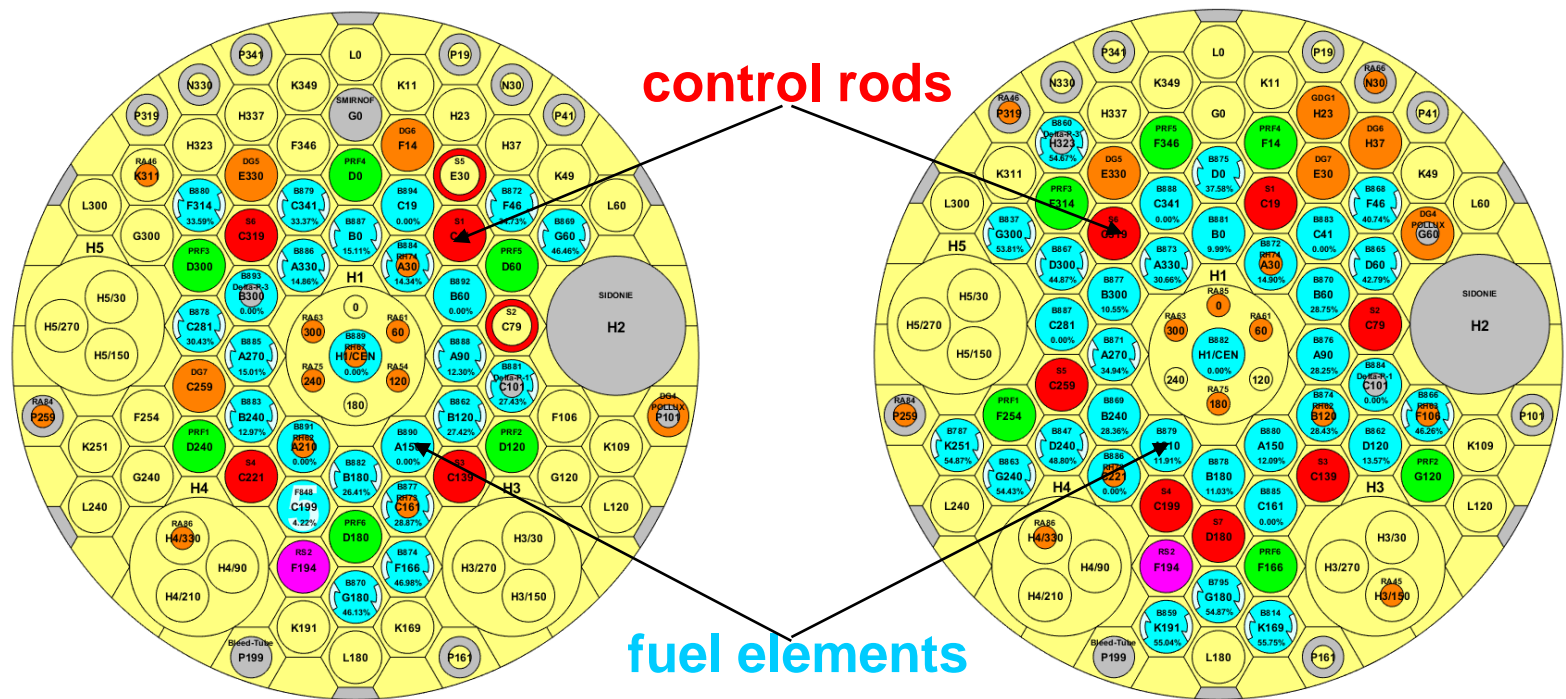
- Hyperboloid core composed of twisted and inclined reactor channels
- HEU core positioned inside and reflected by beryllium matrix
- Flexible BR2 power – 40 to 100 MW
- 6-8 operation cycles per year (each 3-4 weeks long)
- High power density
 - 470 W/cm² nominal
 - 600 W/cm² admissible
- Maximum neutron flux
 - $1,2 \times 10^{15}$ n/cm²/s thermal
 - $8,4 \times 10^{14}$ n/cm²/s fast





Flexible BR2 reactor core loadings

- Variable core configuration – variable number of CR's, FE's
- Fuel elements initial U5 burnup between 0% and 50%



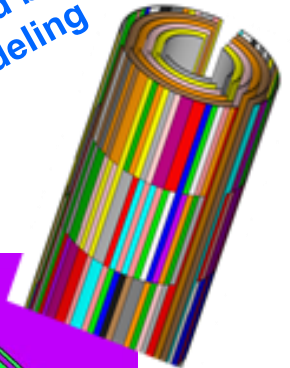
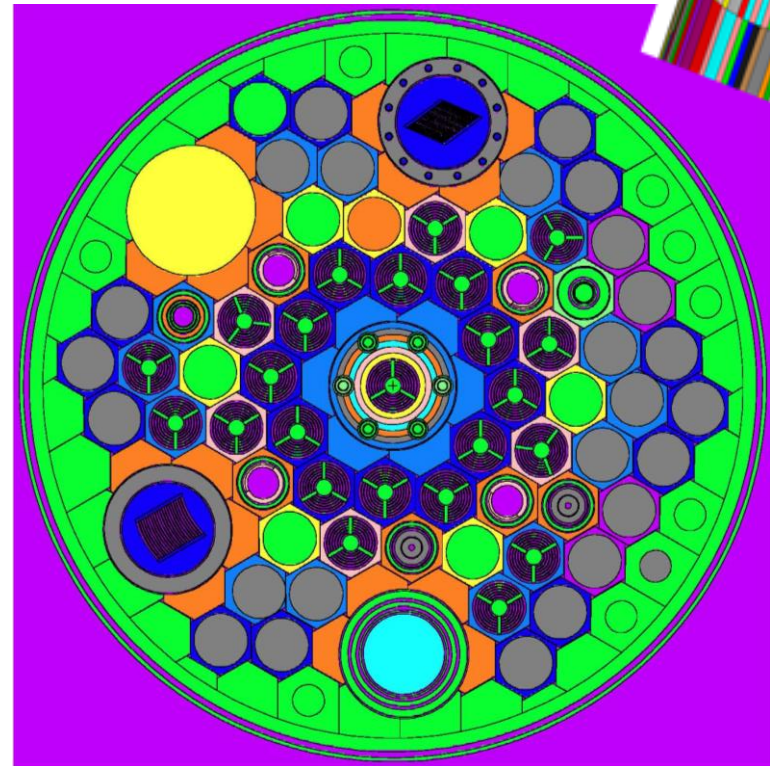
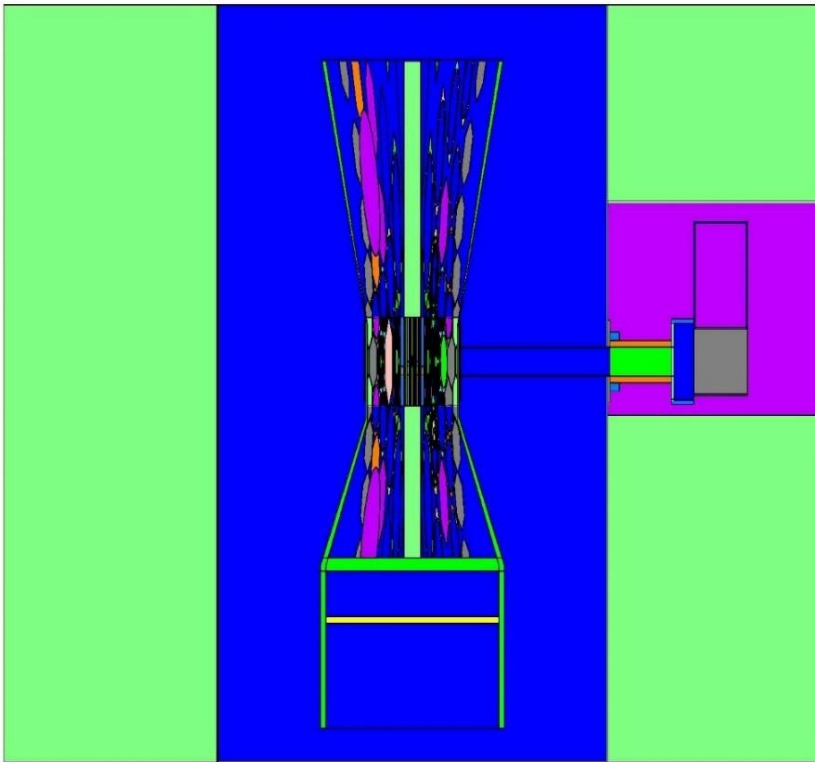
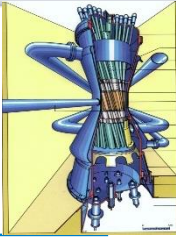
compact core
(4 CR, 20 FE, 40 MW)

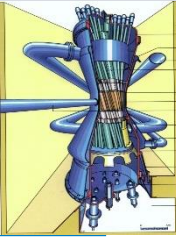
extended core
(6 CR, 30 FE, 60 MW)

MCNP6 3-D full core modeling of BR2

- Automatic burn-up & criticality simulation
- 3-D whole core geometry & depletion
- Follow-up irradiation history of each FA

*twisted hyperboloid bundle
3-D depletion modeling*

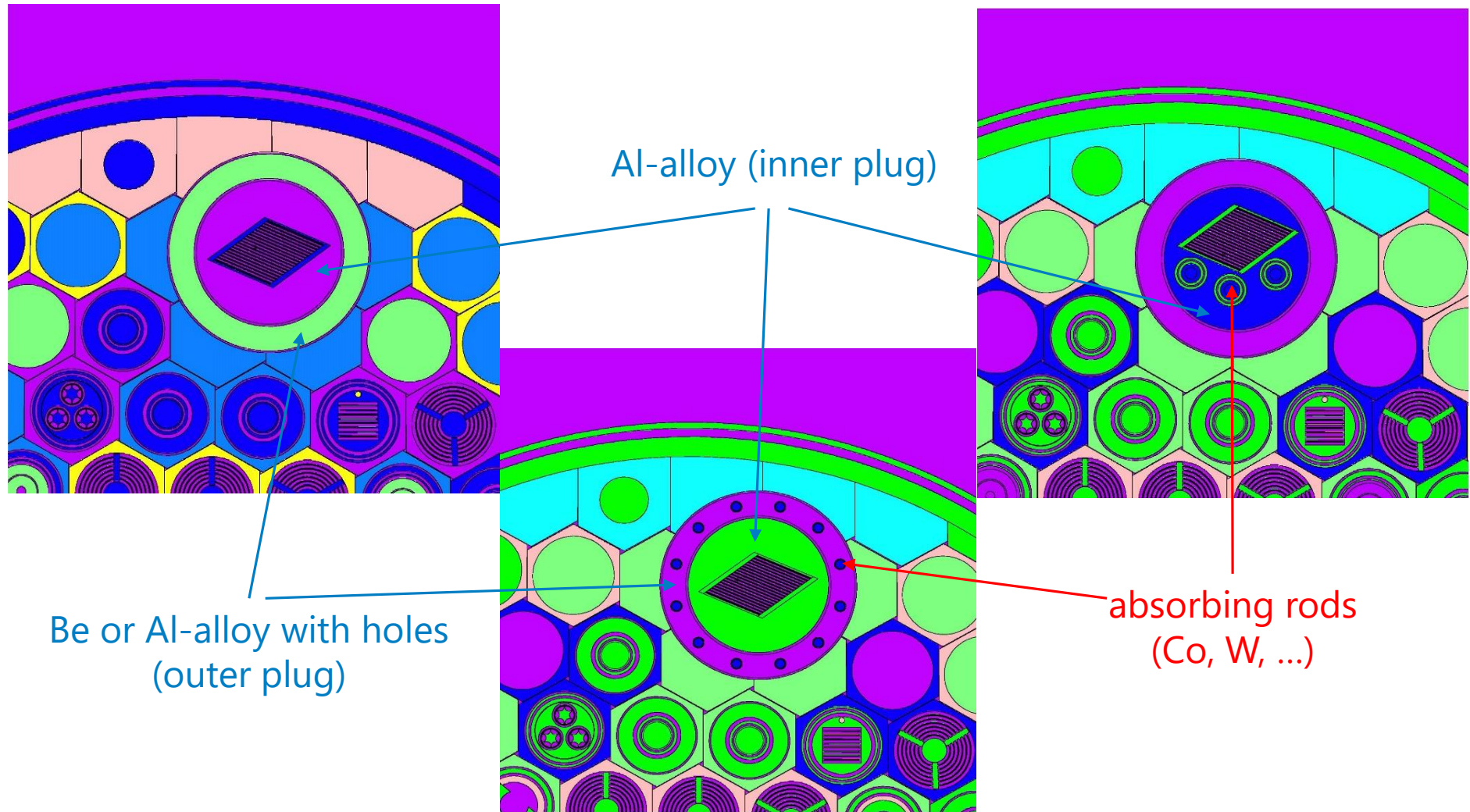
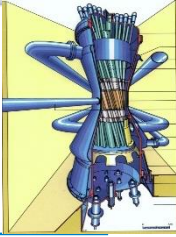




Modeling optimizations for DDE-MITR

- Chosen channel H5 (D=200 mm)
- Optimization of position needed for axial profile
 - Z= -15.28 cm to +43.17 cm
- Special loadings (DG's) in surrounding channels
- Choice of appropriate plug material (Al-alloy, Be)
 - 3 designs for outer plug proposed (Be, Al-alloy, Al-alloy with holes)
 - absorbing rods (Co, W, ..) in inner/outer plug

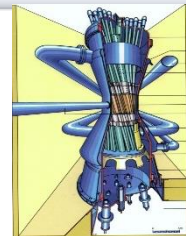
Modeling optimizations for DDE-MITR (cont'd)



Al-alloy (inner plug)

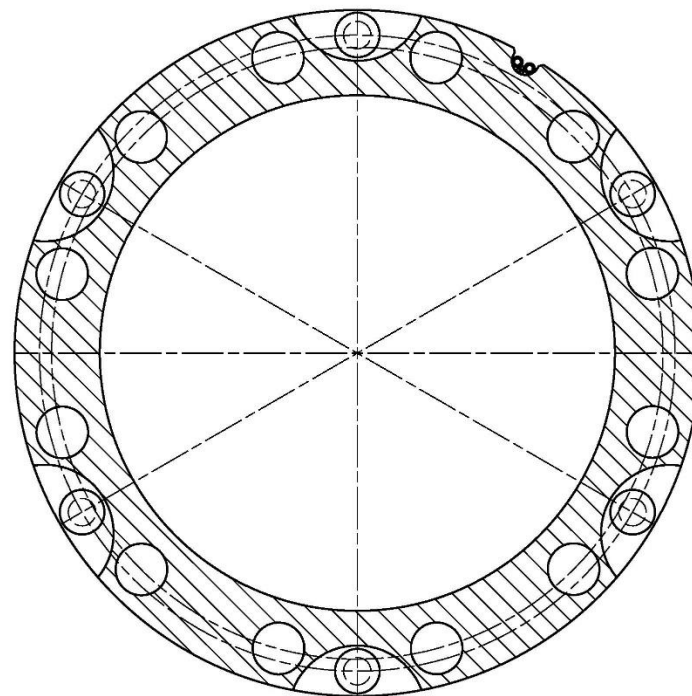
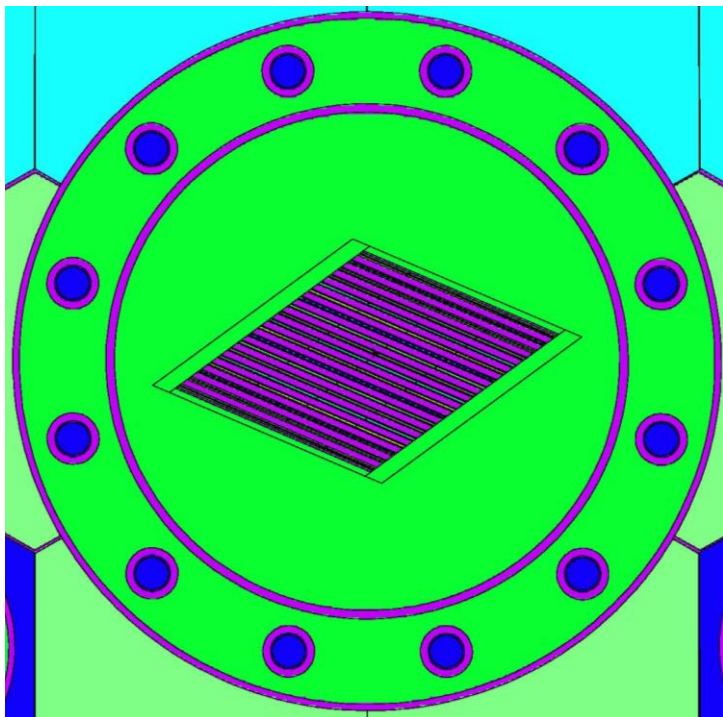
Be or Al-alloy with holes
(outer plug)

absorbing rods
(Co, W, ...)

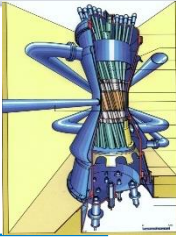


Final design PLUGS for DDE-MITR

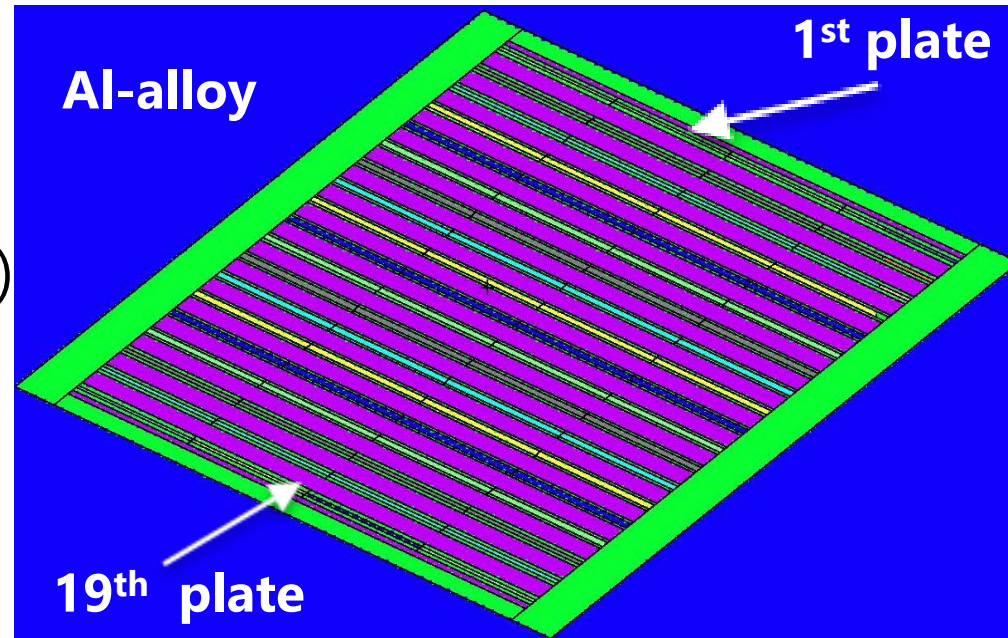
- Inner plug: Al-alloy (to lower the heat flux)
- Outer plug:
 - ❖ Al-alloy with 12 holes filled with rods (Co, W, Al, etc.)



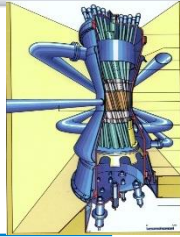
Calculation model of DDE-MITR



- MCNP model of the DDE-MITR-FE contain 19 plates
- Fuel meat thickness varies from 0.33 mm to 0.635 mm
- Each fuel plate modeled with uniform mesh
 - 4 in the transverse direction (13.2 mm wide)
 - 18 in the axial direction (31.6 mm long)
 - Total number of fuel zones: $19 \times 4 \times 18 = \mathbf{1368}$

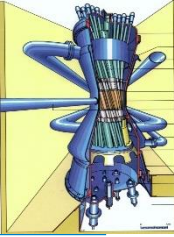


Summary of DDE-MITR-FE parameters

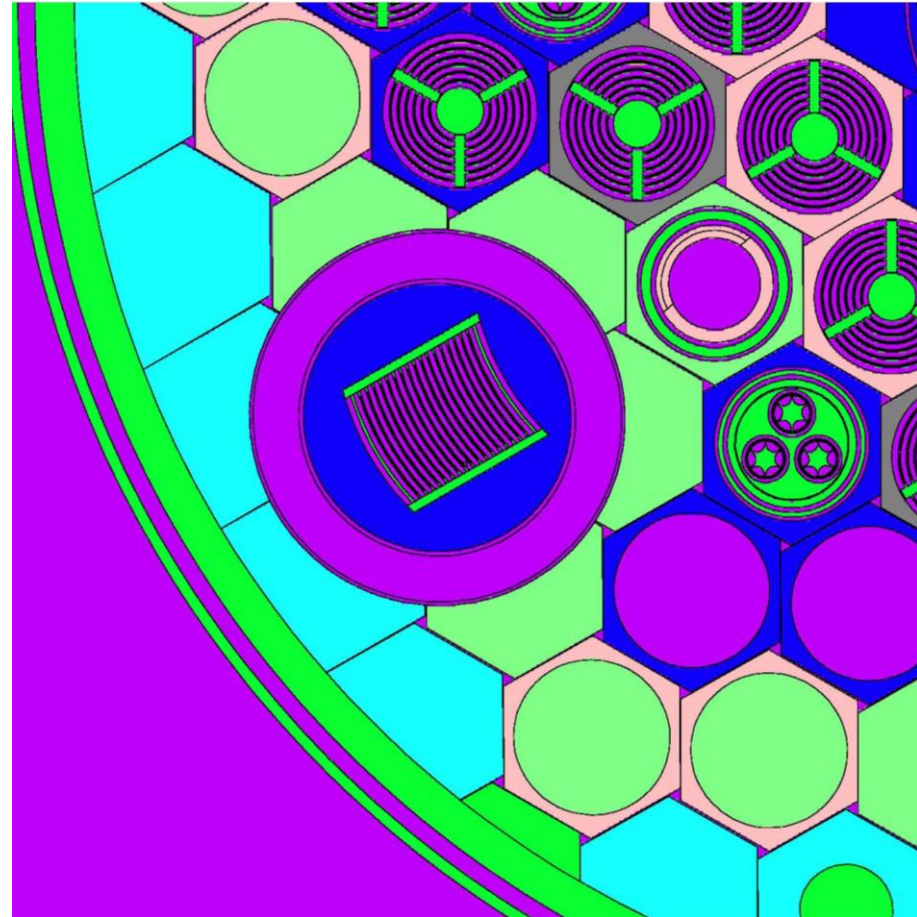


Parameter	value
Axial position in H5 channel relatively to reactor core mid-plane, mm	+123.8
Outer/inner radius of outer fresh Be-plug, mm	99.8/75.0
Radius of inner Al-plug, mm	72.50
U_{total} density, g/cm ³	15.3
U10Mo density, g/cm ³	17.0
²³⁵ U enrichment, %	19.75
²³⁶ U enrichment, %	0.24
Meat thickness of fuel plates 1 & 19, mm	0.33
Meat thickness of fuel plates 2, 3,17 & 18, mm	0.432
Meat thickness of fuel plates 4 to 16, mm	0.635
Plate thickness, mm	1.245
2 exterior water channels thickness, mm	1.618
Plate length, mm	584.200
Meat length, mm	568.325
Diameter of absorbing rods in outer/inner plug, mm	10/20

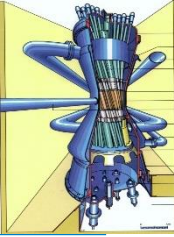
Modeling optimizations for DDE-NBSR



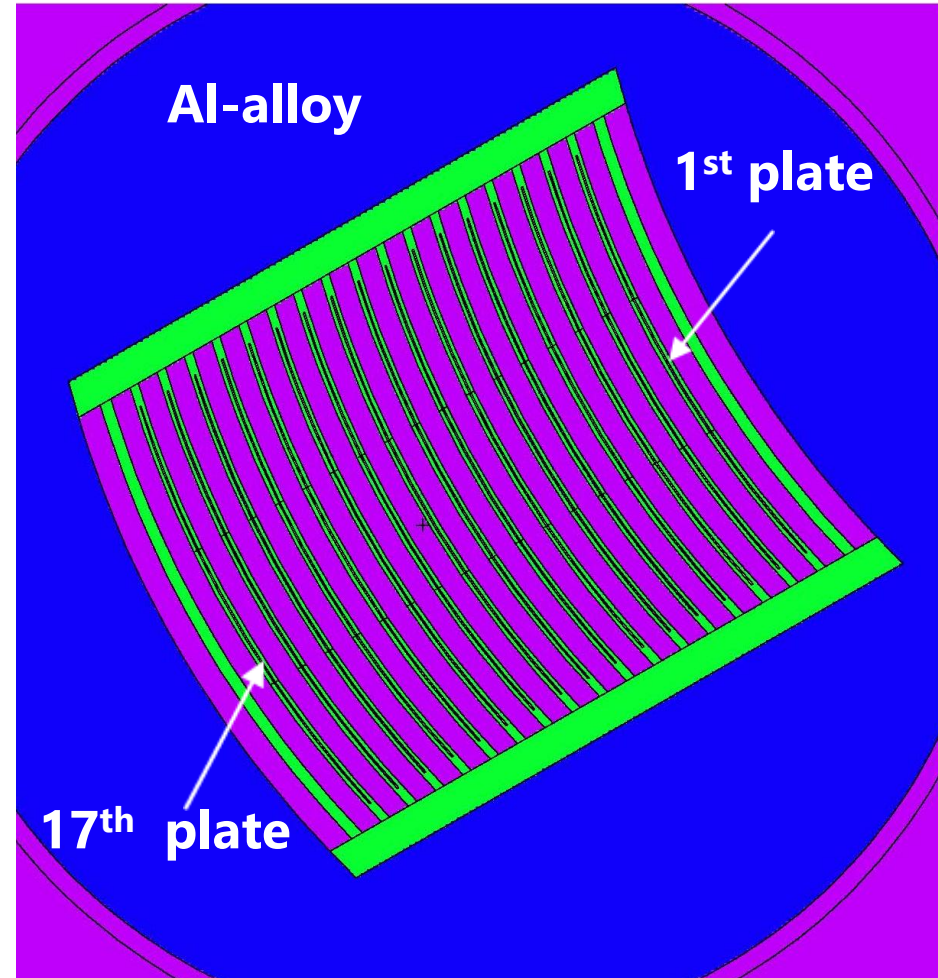
- Chosen channel H3 (D=200 mm)
- Inner plug (Al-alloy)
- Outer plug (Be)
- Optimization of water gap between upper and lower plate
 - water gap=15.24 cm (original design)
 - water gap= 5.24 cm & shift NBSR-FE UP by $\Delta Z=+5$ cm (preferred scenario)
 - water gap= 5.24 cm & shift NBSR-FE DOWN $\Delta Z=-5$ cm



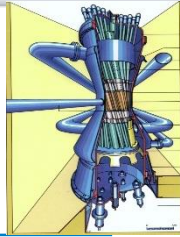
Calculation model of DDE-NBSR



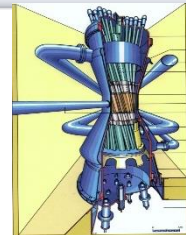
- All fuel plate dimensions not changed (original)
- 17 fuel plates in upper position
- 17 fuel plates in lower position
- 3 azimuth zones in each plate (each ~20 mm long)
- 14 axial zones (each ~20 mm long)
- Total number of fuel zones $2 \times 17 \times 3 \times 14 = \mathbf{1428}$



Summary of DDE-NBSR-FE parameters

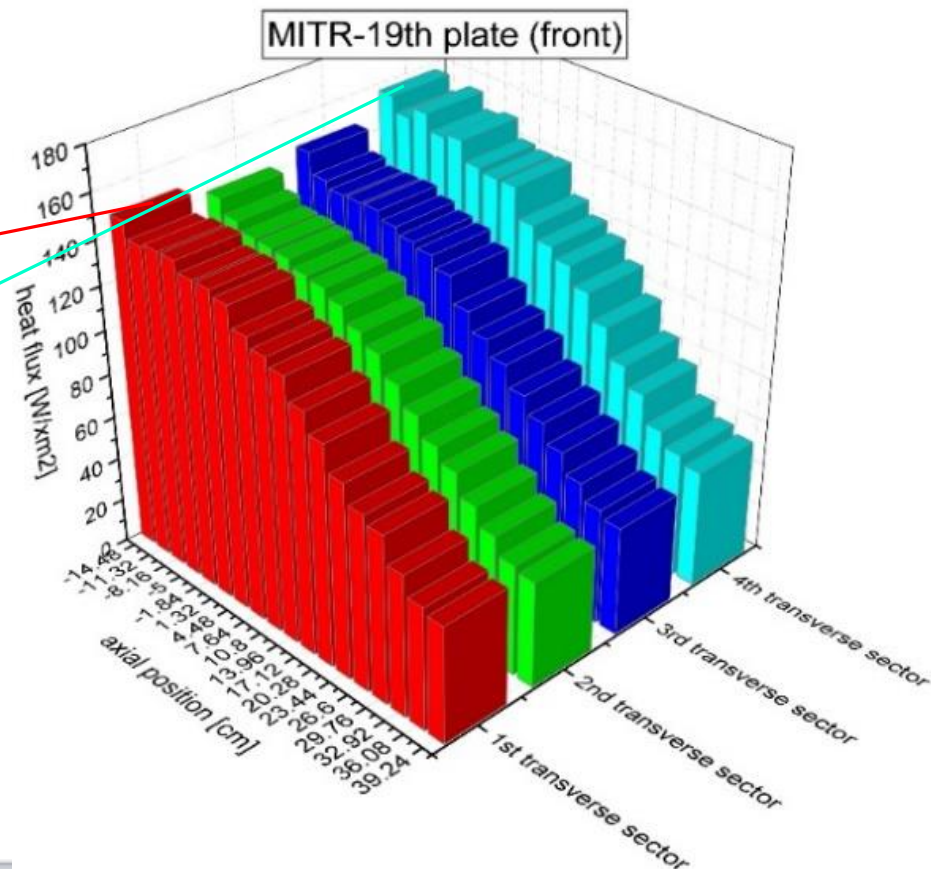
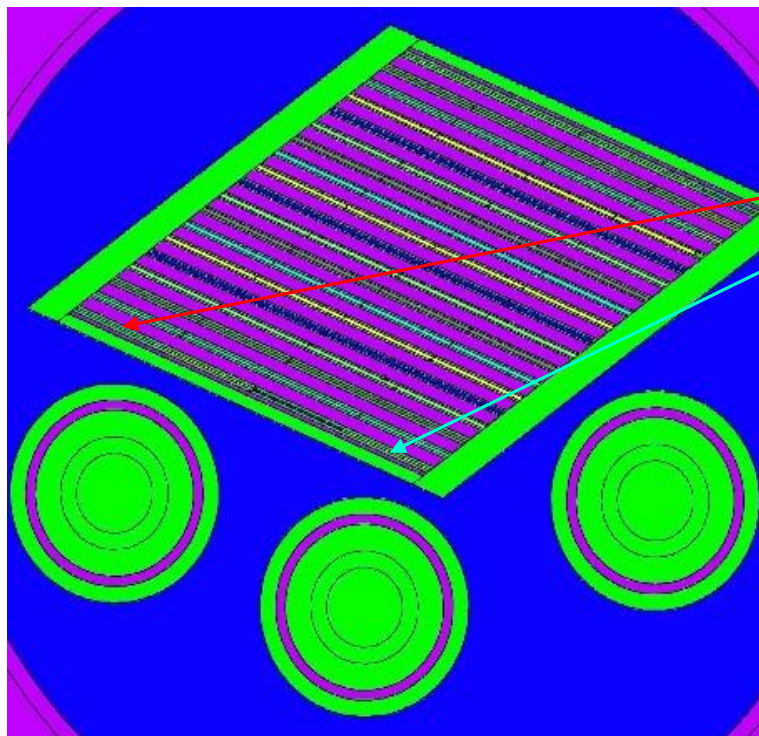


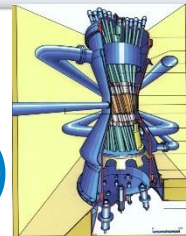
Parameter	value
Axial position in H3 channel relatively to reactor core mid-plane, mm	+100.0
Outer/inner radius of outer fresh Be-plug, mm	99.8/75.0
Radius of inner 60%Al+40%Be-plug, mm	72.50
U_{total} density, g/cm³	15.3
U10Mo density, g/cm³	17.0
²³⁵U enrichment, %	19.75
²³⁶U enrichment, %	0.24
Meat thickness of all (17 lower + 17 upper) fuel plates, mm	0.22
Plate thickness, mm	1.27
36 water channels thickness, mm	2.95
2 dummy exterior plates thickness, mm	1.65
Meat length (upper, lower plate), mm	279.4
Plate length (upper, lower plate), mm	330.2
Water gap between lower and upper plates, mm	52.4



DDE-MITR: Heat flux at BOL (Al rods inner plug)

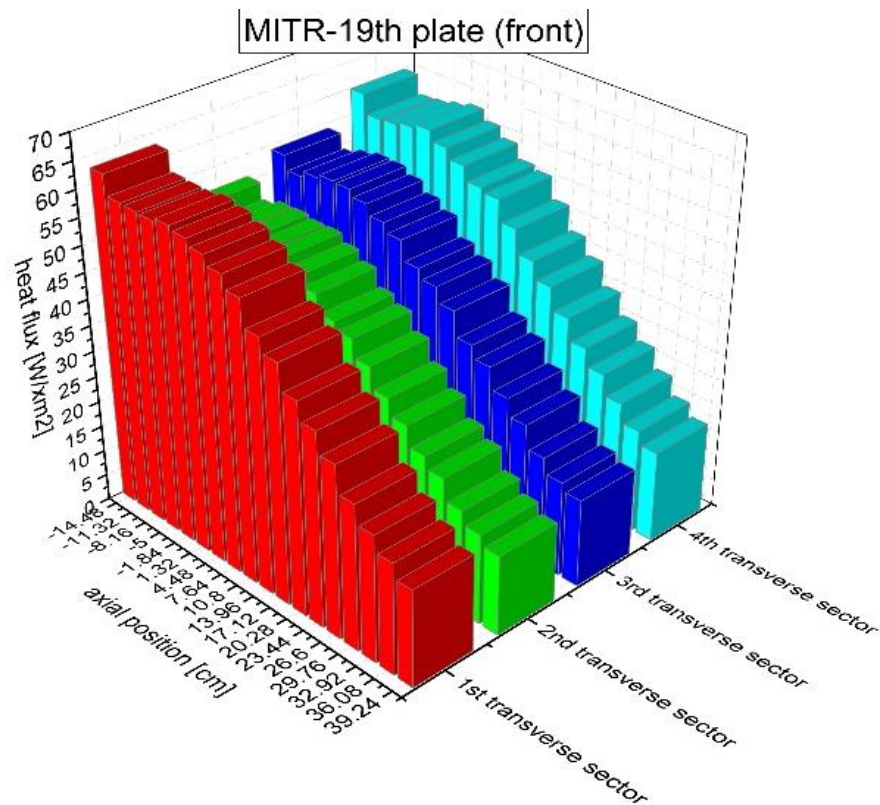
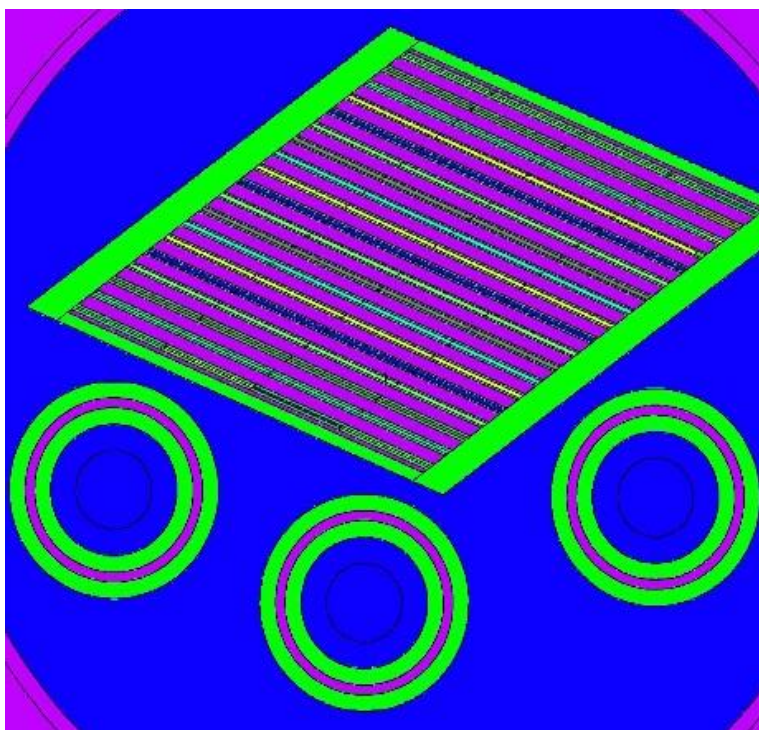
- Be (outer plug), Al-alloy (inner plug)
- $Q_{\max} = 158 \text{ W/cm}^2$; $Q_{\min} = 31 \text{ W/cm}^2$

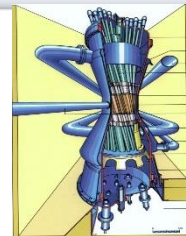




DDE-MITR: Heat flux at BOL (Co, W rods inner plug)

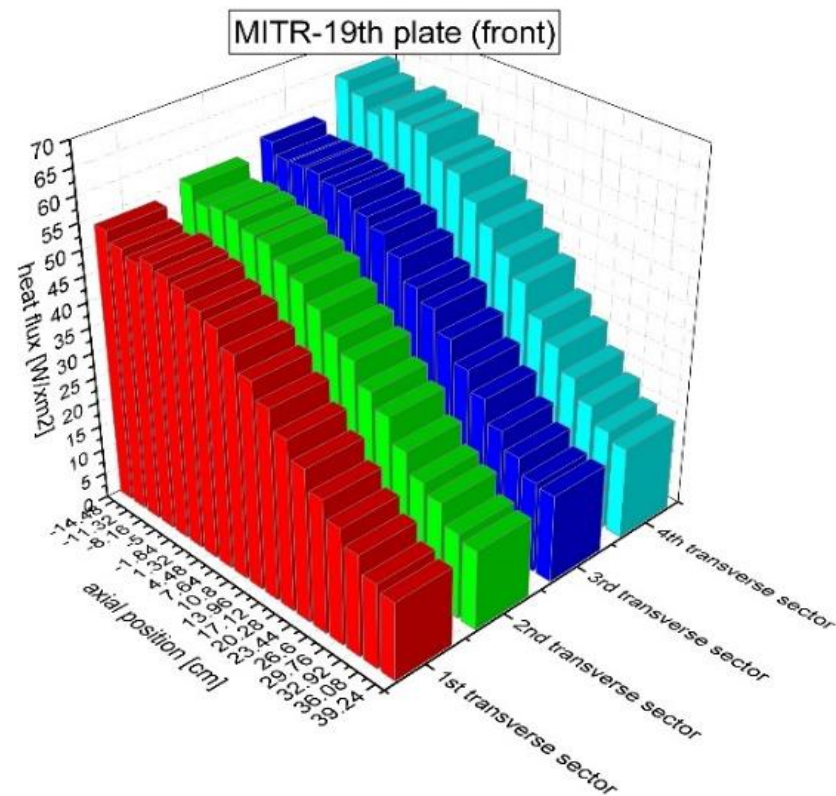
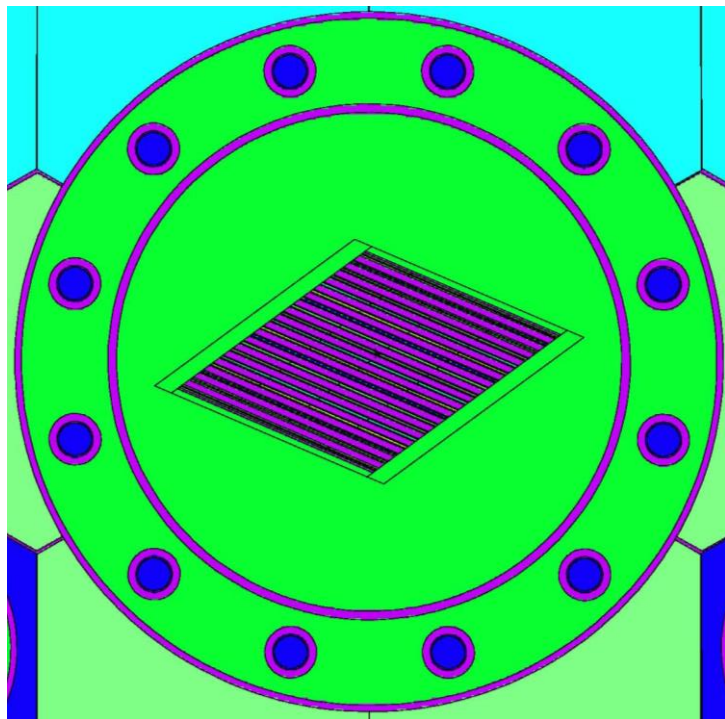
- Be (outer plug), Al-alloy (inner plug)
- $Q_{\max} = 65 \text{ W/cm}^2$; $Q_{\min} = 15 \text{ W/cm}^2$

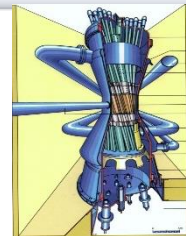




DDE-MITR: Heat flux at BOL (Co, W rods outer plug)

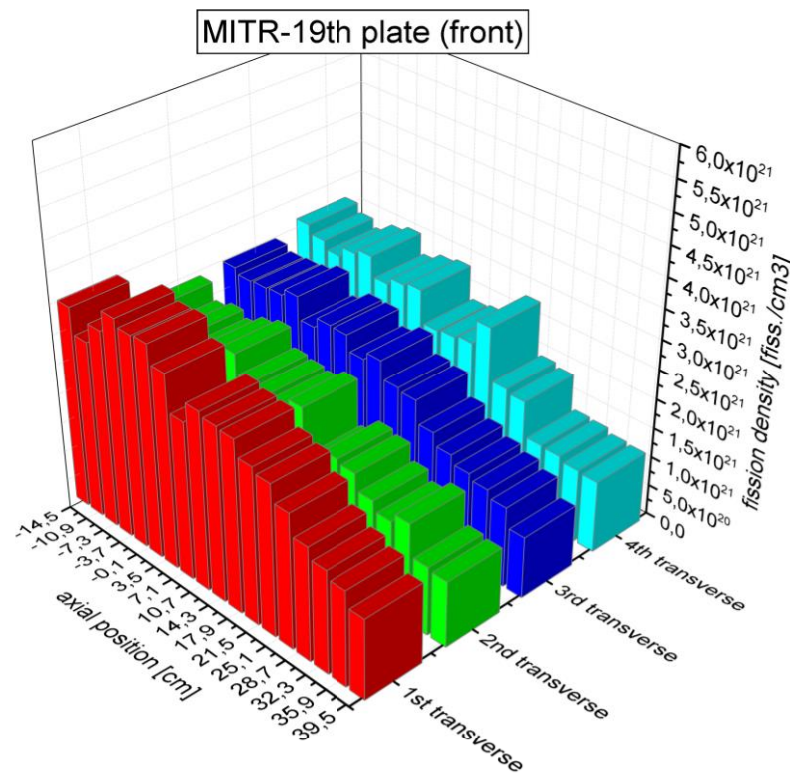
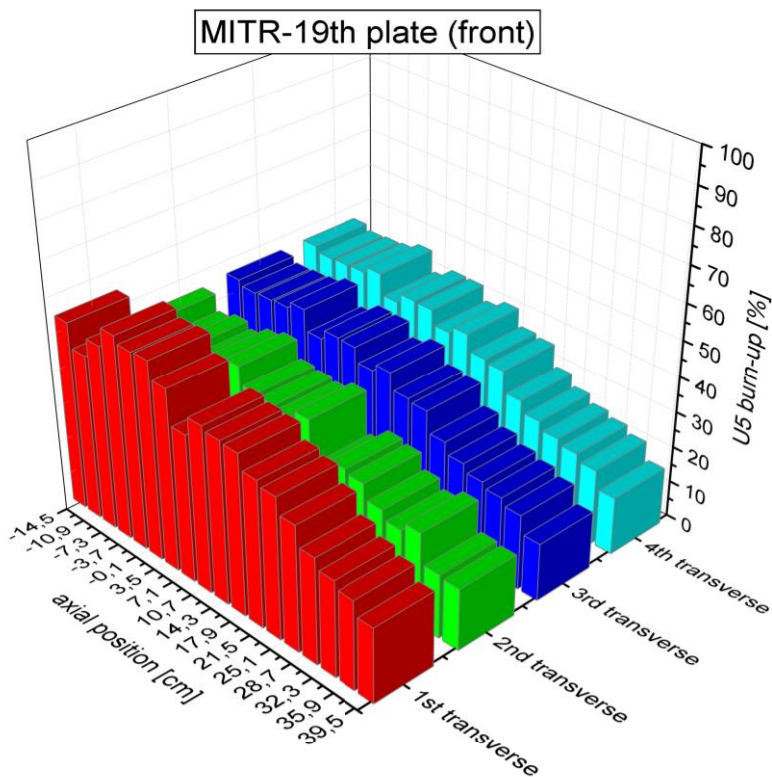
- Proposed geometry design: Al-alloy (inner & outer plug)
- $Q_{\max} = 67 \text{ W/cm}^2$; $Q_{\min} = 16 \text{ W/cm}^2$

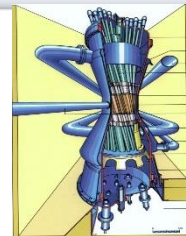




DDE-MITR: Burn-up at 250 F.P.D. ~ BR2 10 cycles

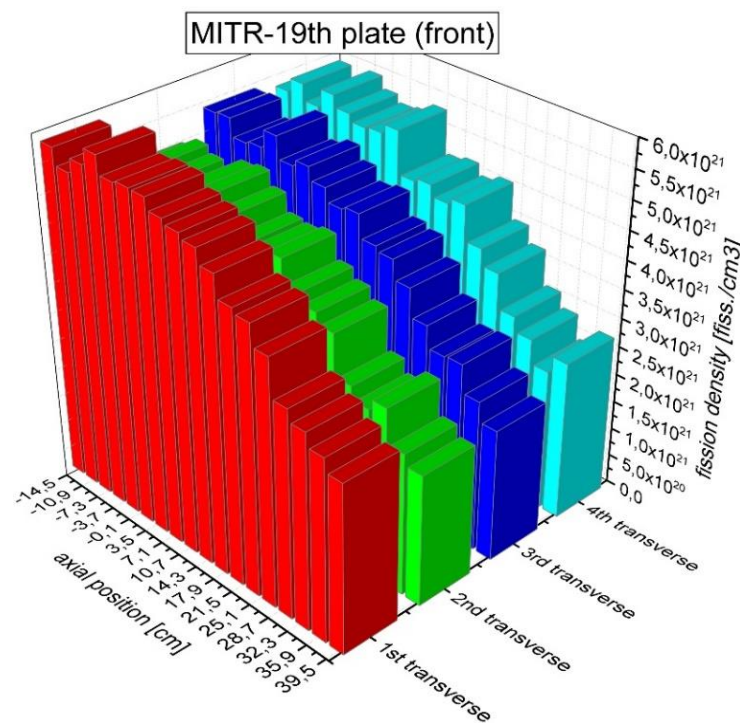
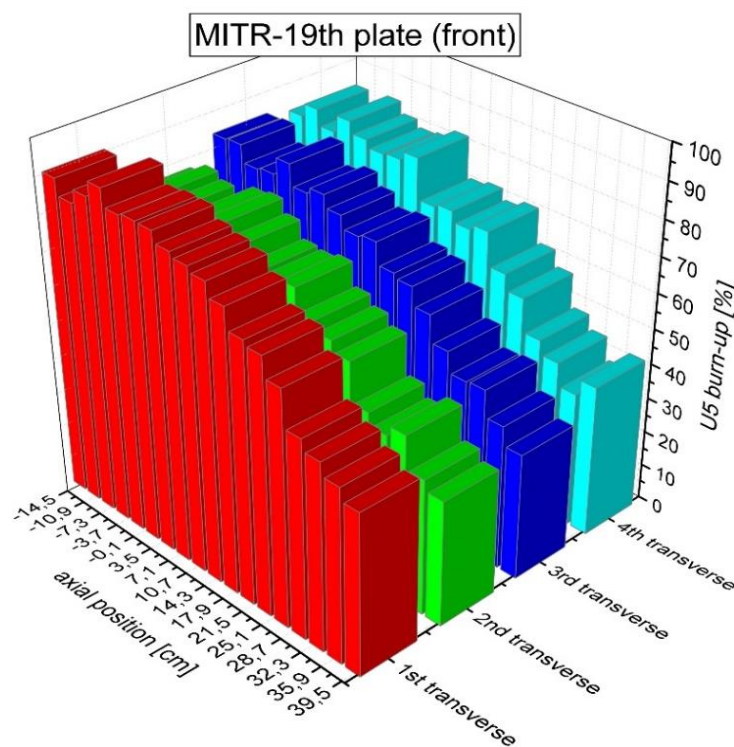
- Axial distributions at 250 days for proposed design
 - Maximum U5 burn-up: 55%
 - Maximum fission density: $3,5E21$ fiss./cm³



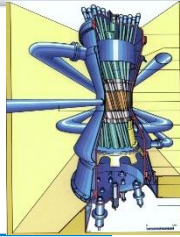


DDE-MITR: Burn-up at 630 F.P.D. ~ BR2 26 cycles

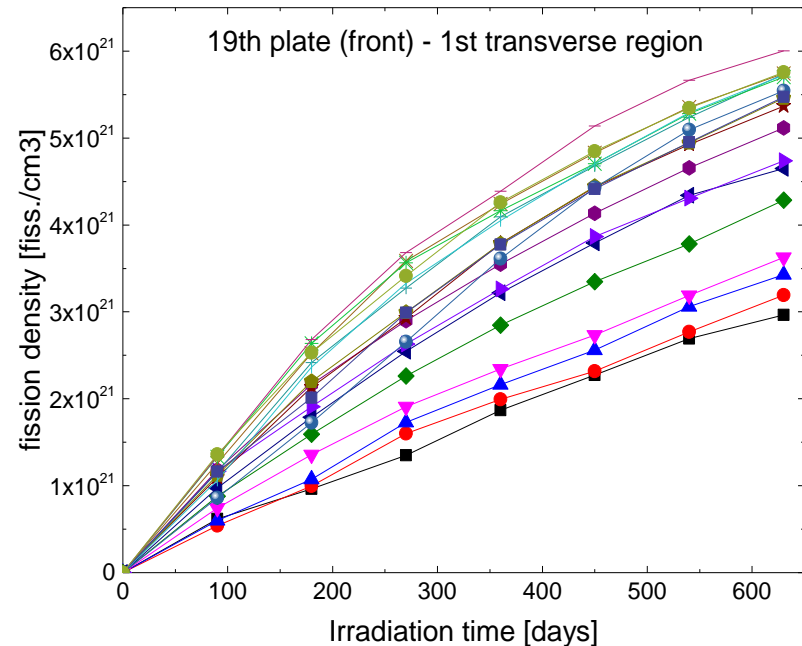
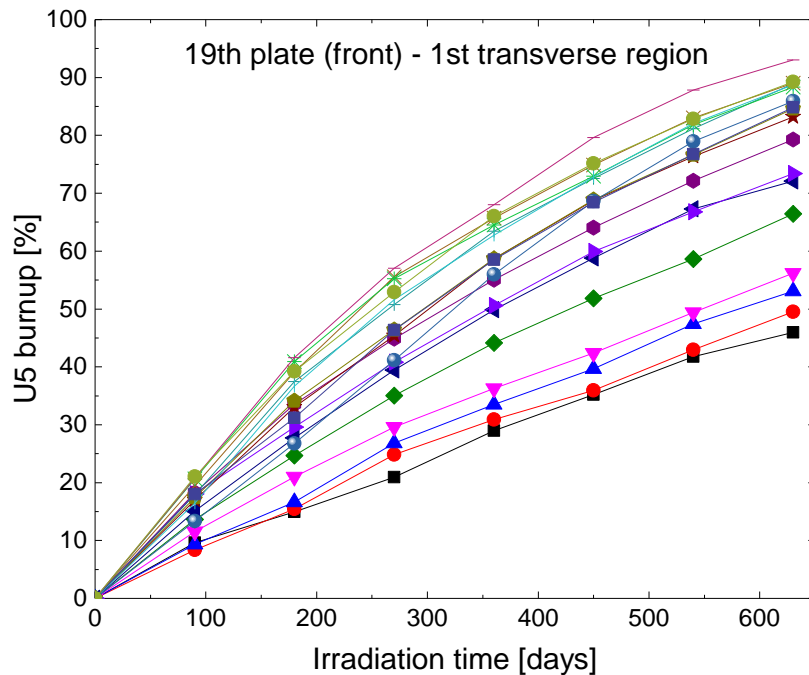
- Axial distributions at EOL for proposed design
 - Maximum U5 burn-up: 90%
 - Maximum fission density: $5,8E21$ fiss/cm³

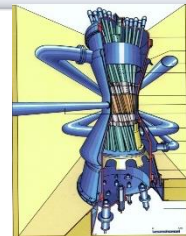


DDE-MITR: Burn-up evolution (proposed design)



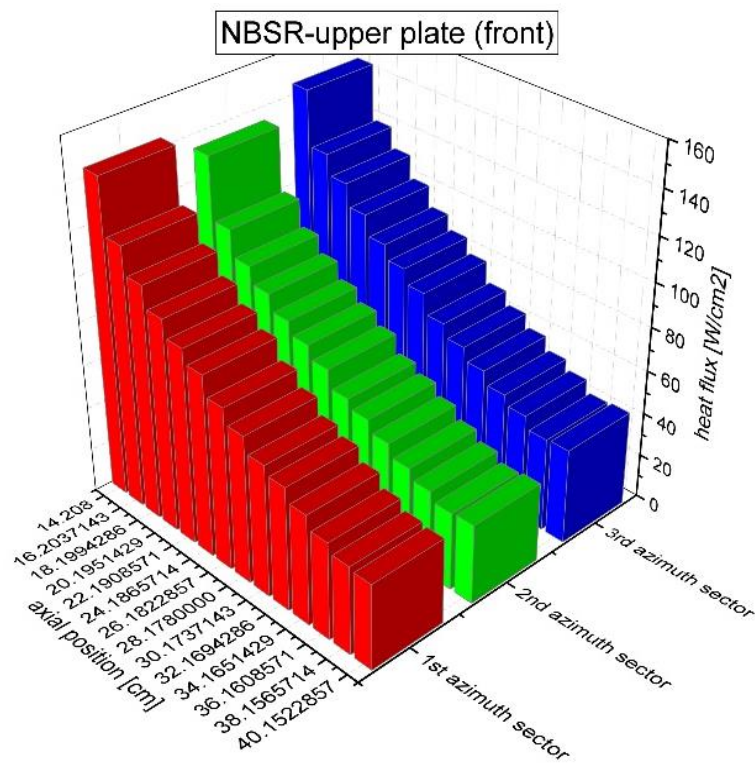
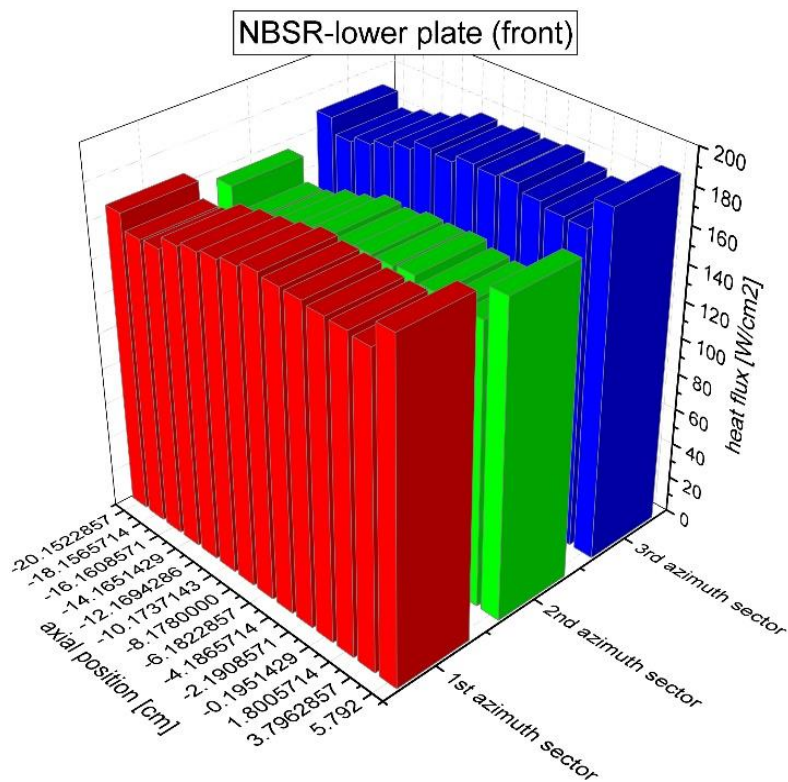
- Time evolution of U5 burn-up (left) and fission density (right) during ~ 26 BR2 operation cycles:
 - scenario with cobalt rods inner/outer plug
 - for $Q_{\max} = 67 \text{ W/cm}^2$ at BOL



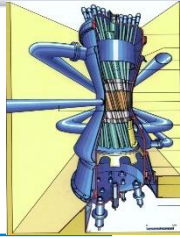


DDE-NBSR: Heat flux at BOL

- BOC #1
- $Q_{\max} = 180 \text{ W/cm}^2$; $Q_{\min} = 155 \text{ W/cm}^2$ (lower plate)
- $Q_{\max} = 145 \text{ W/cm}^2$; $Q_{\min} = 40 \text{ W/cm}^2$ (upper plate)

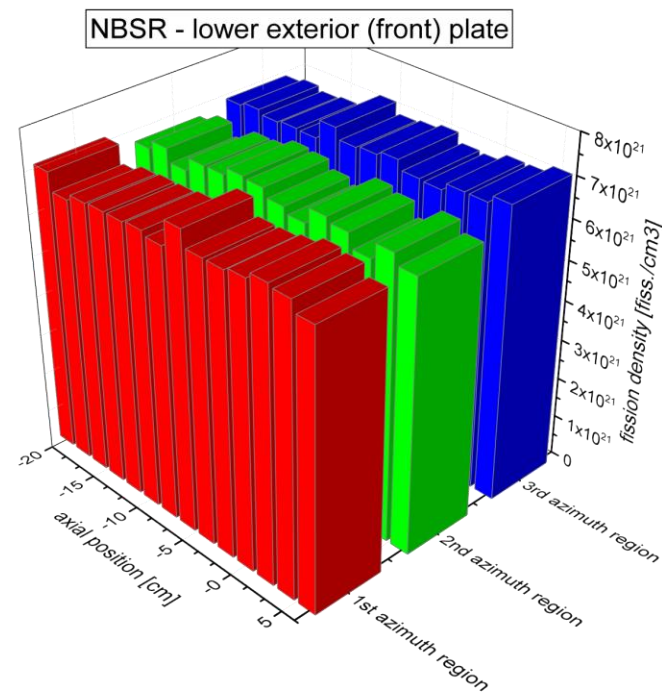
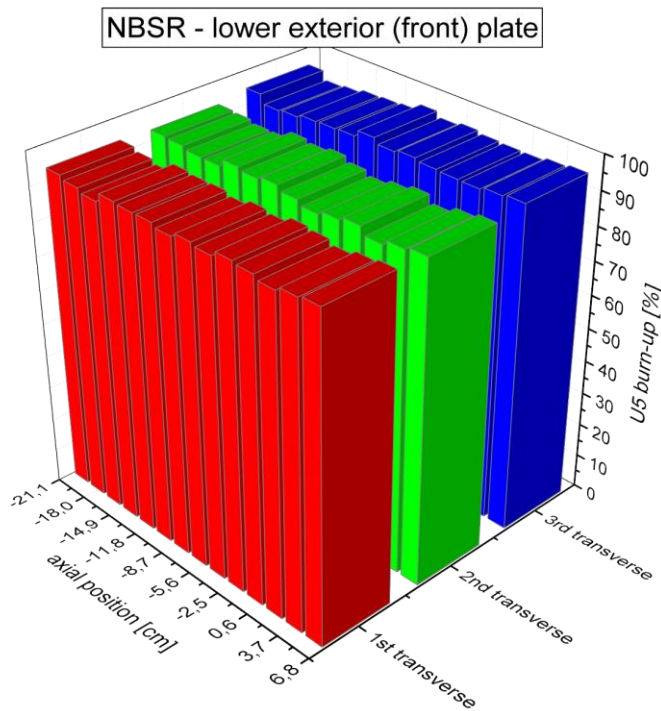


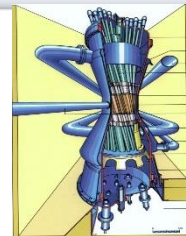
DDE-NBSR: Burn-up at 350 F.P.D. ~ BR2 15 cycles



- Axial distributions for proposed design

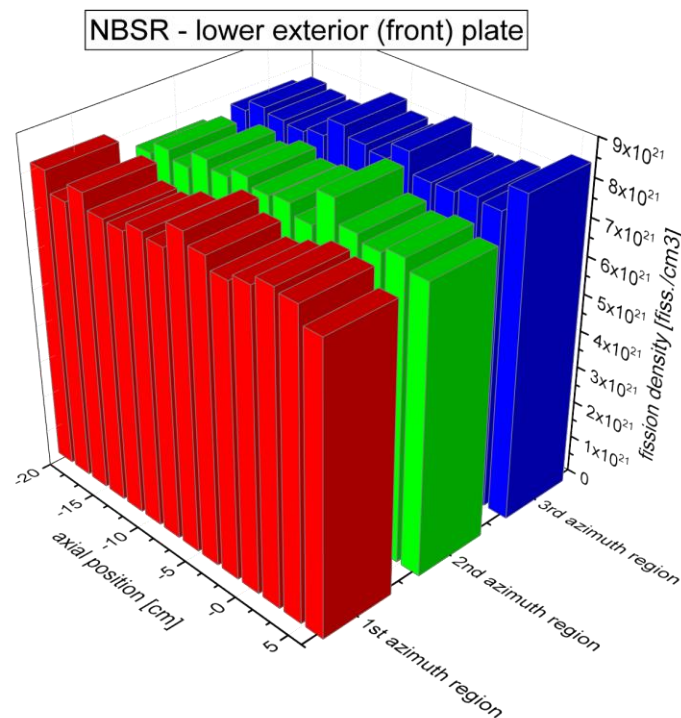
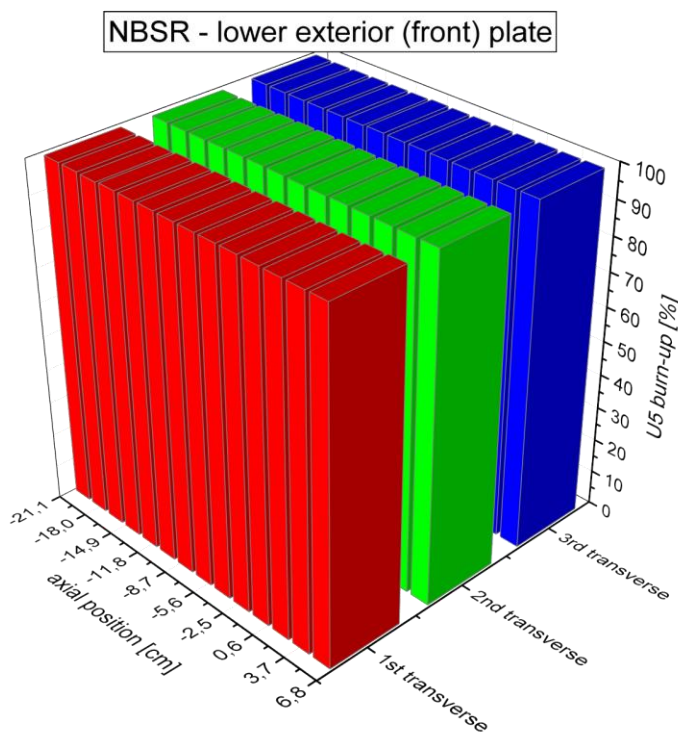
- ❖ Maximum U5 burn-up: > 90%
- ❖ Maximum fission density: $7,2E21$ fission/cm³



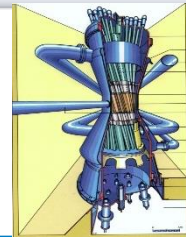


DDE-NBSR: Burn-up at 600 F.P.D. ~ BR2 25 cycles

- Axial distributions at EOL for proposed design
 - ❖ Maximum U5 burn-up: 100%
 - ❖ Maximum fission density: $8,4E21$ fiss./cm³

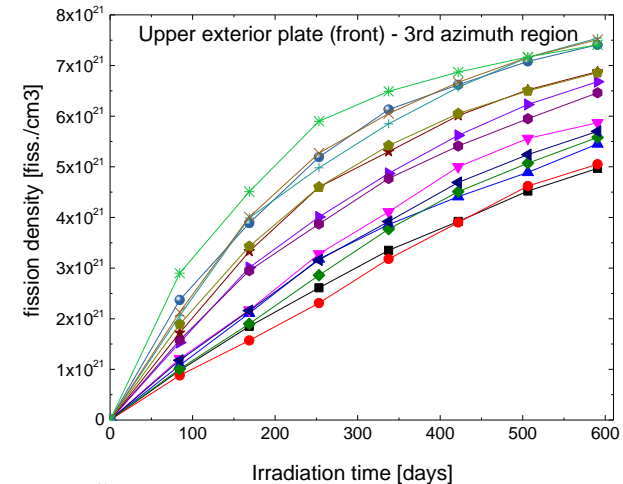
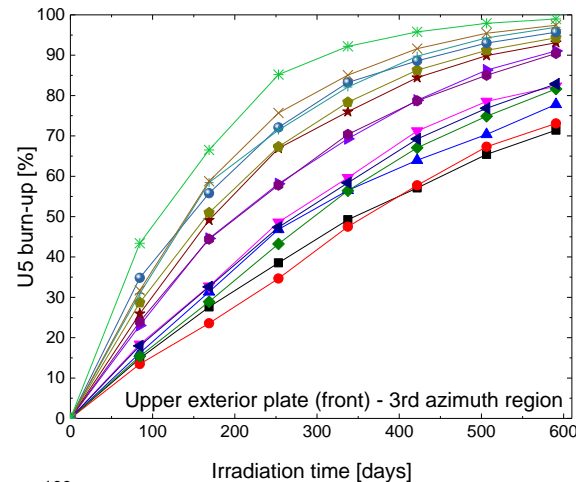


DDE-NBSR: Burn-up evolution during 25 cycles

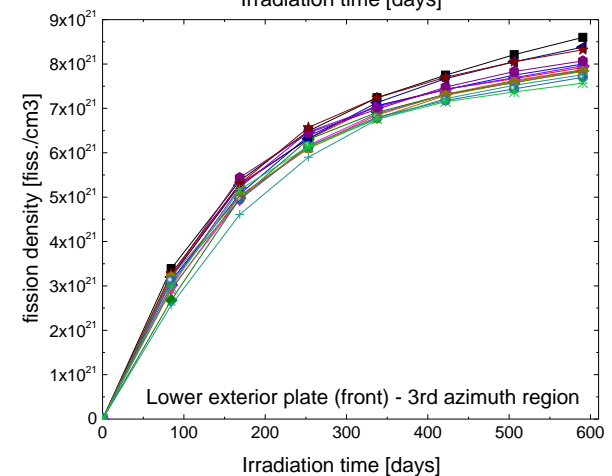
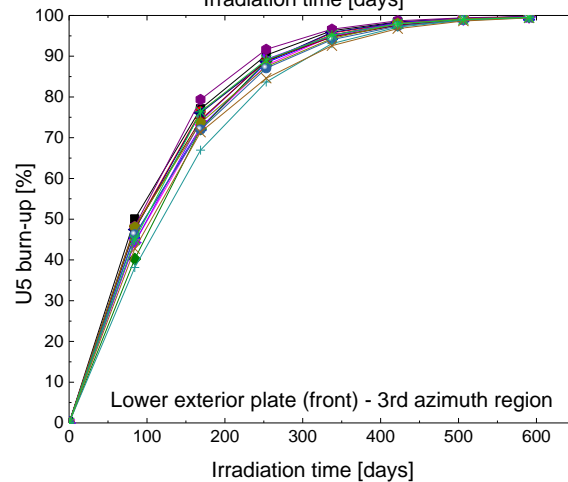


- Time evolution of U5 burn-up (left) and fission density (right)

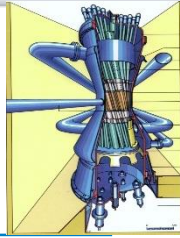
❖ upper plate



❖ lower plate



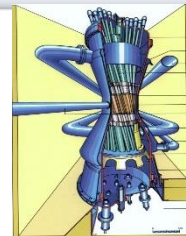
Summary



● DDE-NBSR

- Location in one of the 200 mm diameter channels (H3, H4 or H5)
- Reduced water gap between upper and lower fuel plates
- Use of pure Be-outer plug and Al-alloy for inner plug
- Negligible reactivity effect of DDE-NBSR vs. standard Be-plug
- **Target performances (BOL) are met: $Q_{\max} = 170 \text{ W/cm}^2$**
- **Target performances (EOL)**
 - ❖ **~12-15 cycles > 90% U5 burn-up, $7,2\text{E}21 \text{ fiss/cm}^3$**
 - ❖ **~15-25 cycles saturation of U5 burn-up, $8,4\text{E}21 \text{ fiss/cm}^3$**

➔ 12 cycles sufficient for maximum fission density $\leq 7\text{E}21 \text{ fiss/cm}^3$



Summary (cont'd)

● DDE-MITR

- Location in one of the 200 mm diameter channels (H3, H4 or H5)
- Negligible reactivity effect of DDE-MITR vs. standard Be-plug
- Loading of absorbing devices in surrounding channels
- Inner plug Al-alloy
- Outer plug: Be or Al-alloy with holes for absorber rods (Co, W)
- **Target performances (BOL) are met: $Q_{\max} = 65 \text{ W/cm}^2$**
- **Target performances (EOL) are met: $F_{\max} = 5.8\text{E}21 \text{ fiss/cm}^3$**
 - ❖ **25-26 BR2 cycles for $Q_{\max}(\text{BOC1}) = 65 \text{ W/cm}^2$**
 - ❖ **< 20 BR2 cycles if maintain $Q_{\max}(\text{BOCi}) = 65 \text{ W/cm}^2$ in cycles 'i'**
 - ❖ **< 20 BR2 cycles if increase target heat flux**

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