



IANUS

Interdisciplinary Research Group

Science, Technology and Security



**TECHNISCHE
UNIVERSITÄT
DARMSTADT**

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Neutronic Calculations for Conversion of One-Element-Cores from HEU to LEU Using Monolithic UMo Fuel

Funded by Berghof Foundation for Conflict Research, Berlin

*11th International Topical Meeting on Research Reactor
Fuel Management (RRFM),
11-15 March 2007, Lyon, France*

Performance Analysis

Not only maximum flux and cycle length

Performance of a research reactor (beam type) is a function of

- Available beam time per year (cycle length and downtime)
- Number and efficiency of neutron guides and experiments
- Available flux at experiments

Best approach:

Modelling from the source to the experiment

Coupling of instrumentation codes (e.g. MCSTAS, VITESS) to the reactor code?

Also for other reactors:

Maybe flux losses can be compensated by improving neutron guides and experiments (e.g. ILL, Petten et al.) (economic benefits !?)

FRM-II Principal Conversion Options

Obligation to convert to at least 50% enrichment or below by end of 2010
(according to scientific-technological possibilities)

UMo Dispersion

8 g/cc

50% enrichment

~8% flux losses

(LEU impossible)

UMo Monolithic

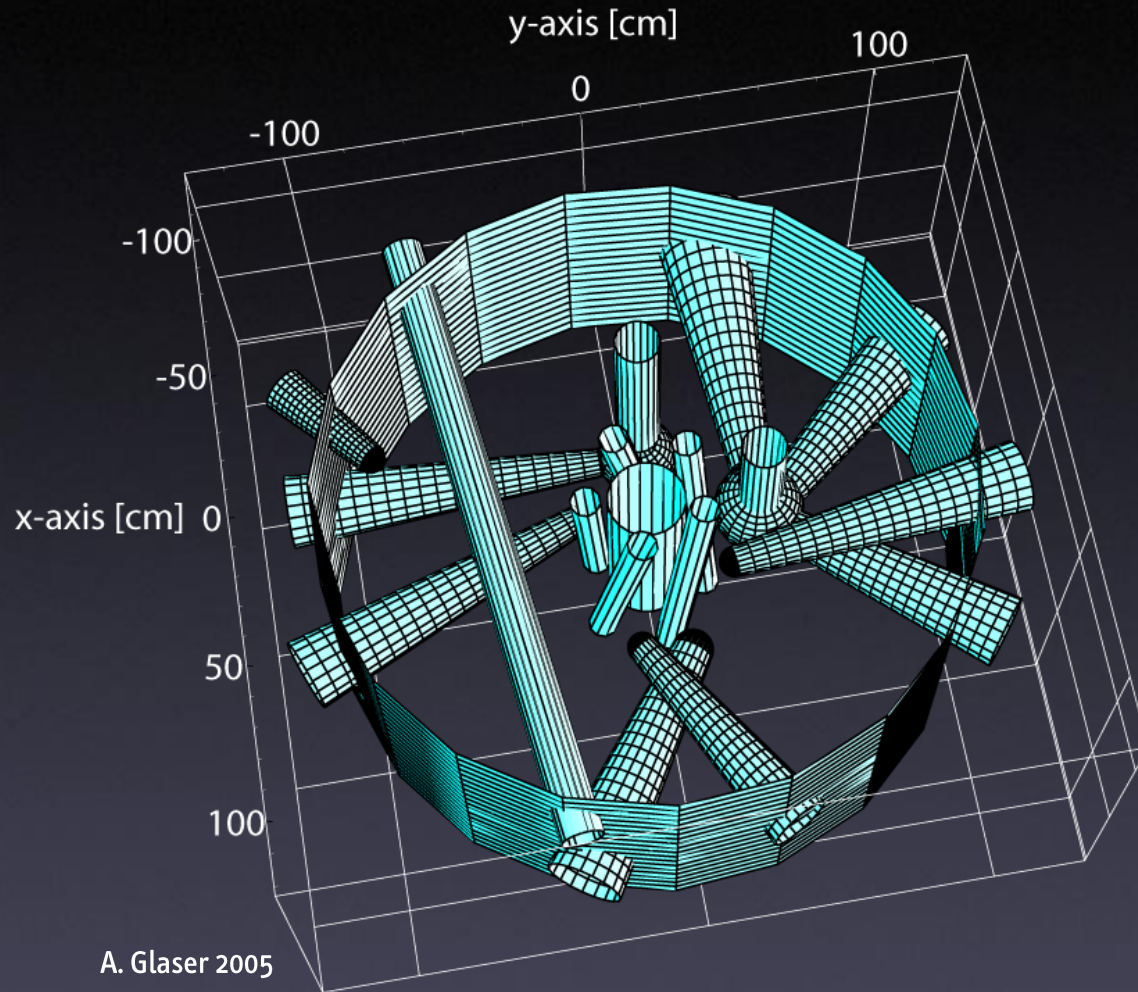
16 g/cc

< 33 % enrichment

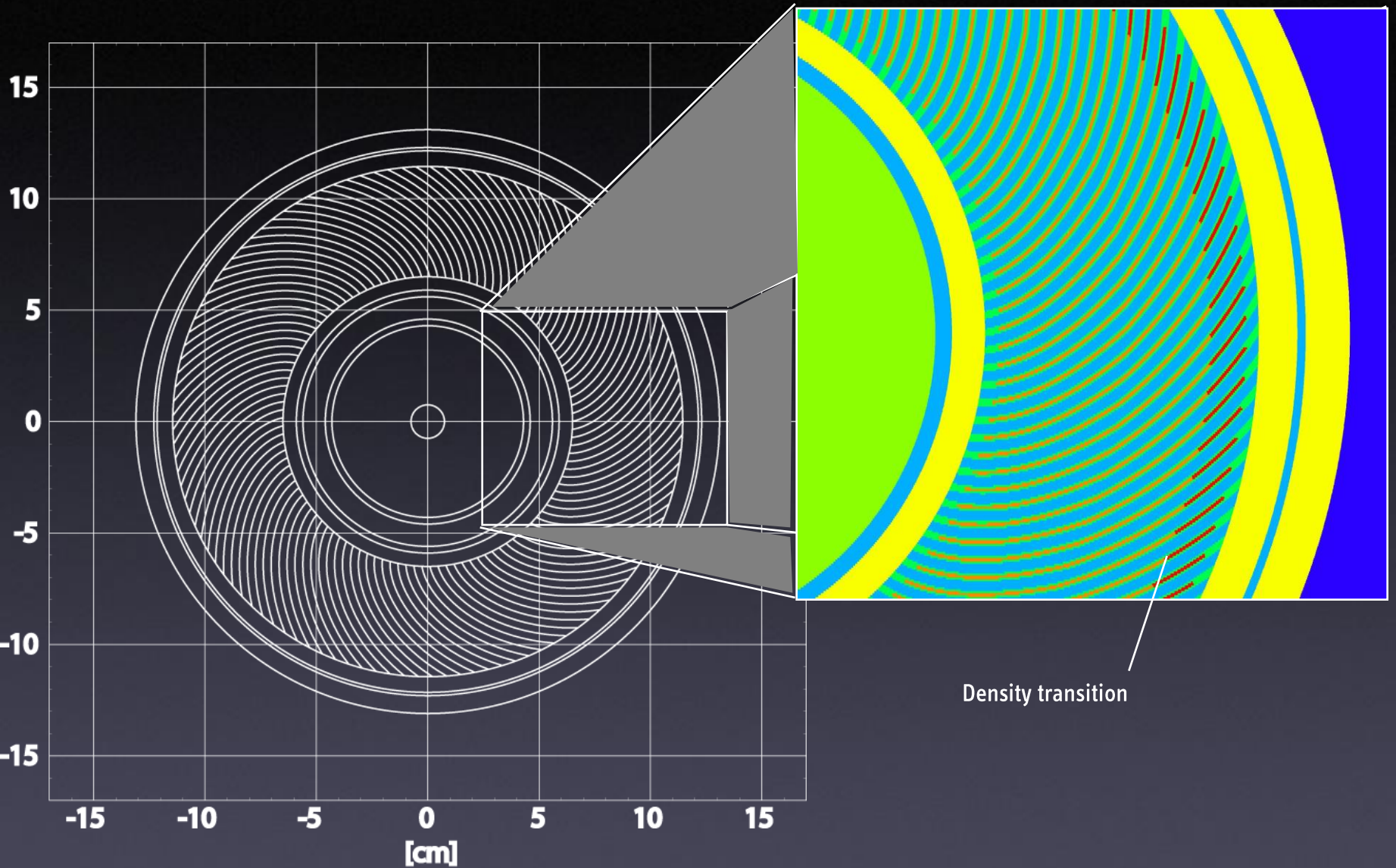
potential for LEU ?!

this talk

Reactor



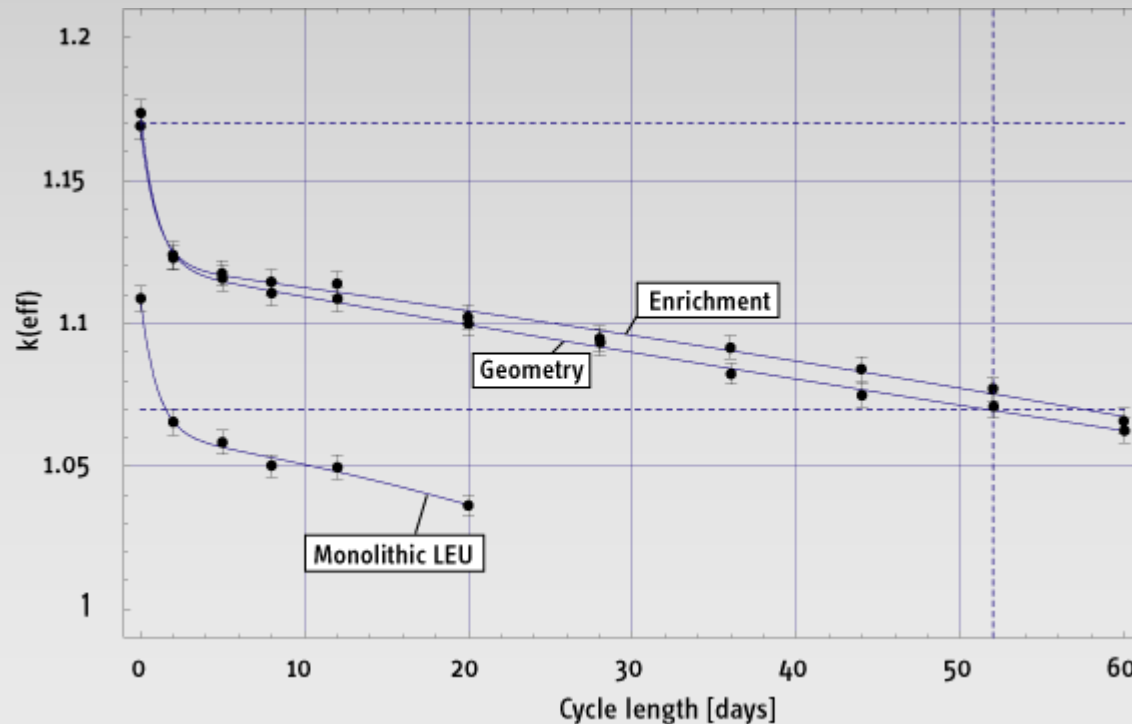
Fuel Element Model



Increasing Initial Reactivity

	Enrichment	Enrichment + Geometry
Thermal Power	20 MW	20 MW
Fuelled height of core	70 cm	80 cm
Required Enrichment	32-33%	26-27%

Elongation of active height



-> $k_{eff,ini} \sim 1.17$

Non-proliferation objective ?

Cycle Length of the FRM-II core for the current HEU design and for monolithic fuel with 16 g/cm³ in the current HEU design geometry.

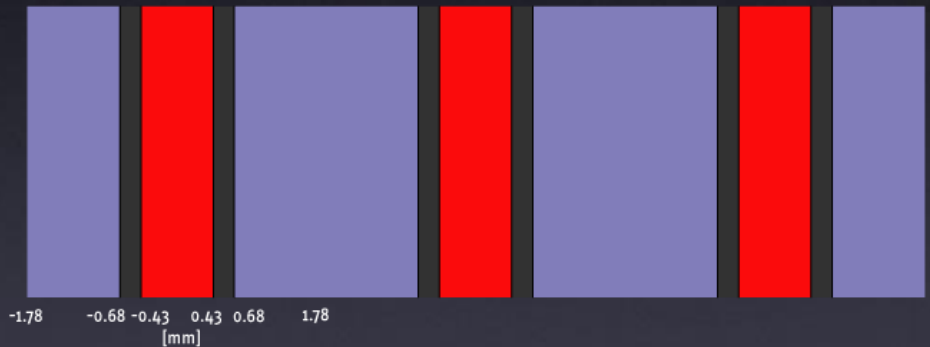
Geometrical Changes I

Constant Number of
Plates in the core

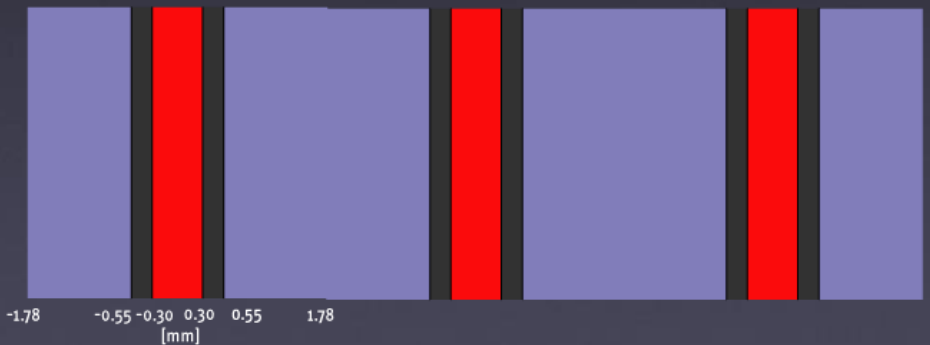
Current Geometry



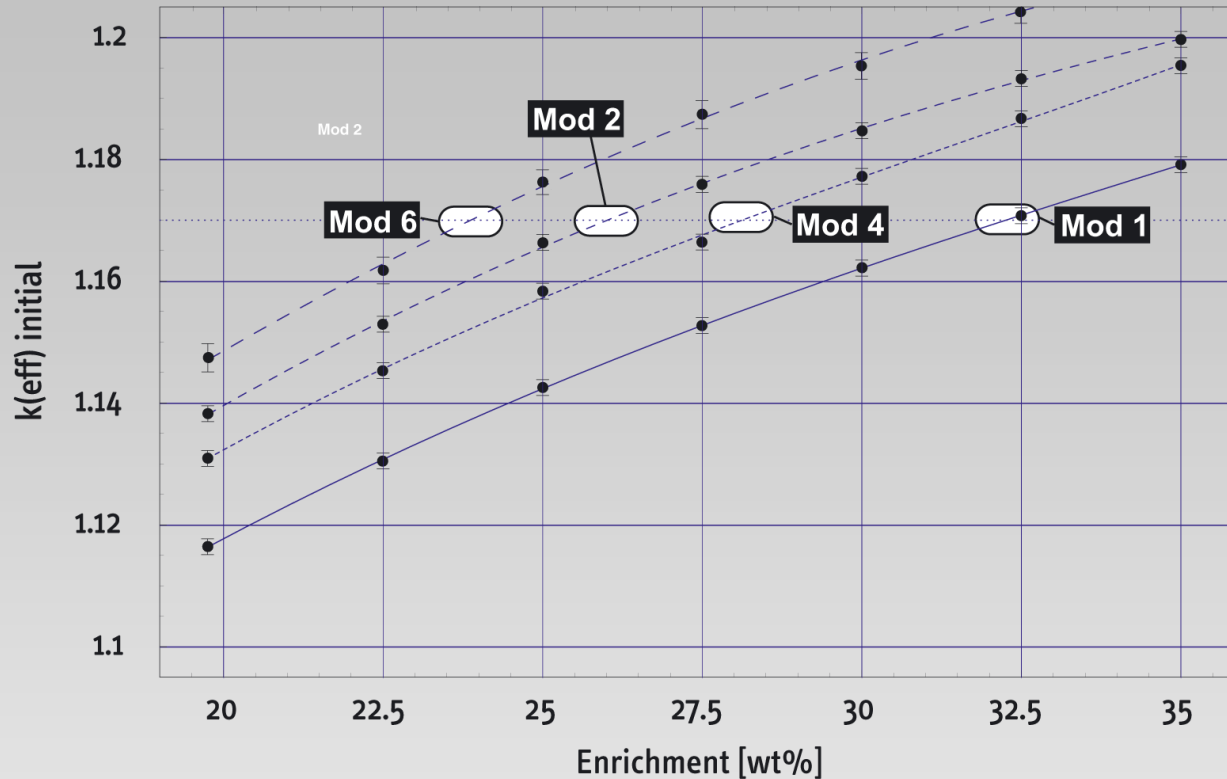
Thinner Cladding
Thicker Meat



Thinner Cladding
Wider cooling channels

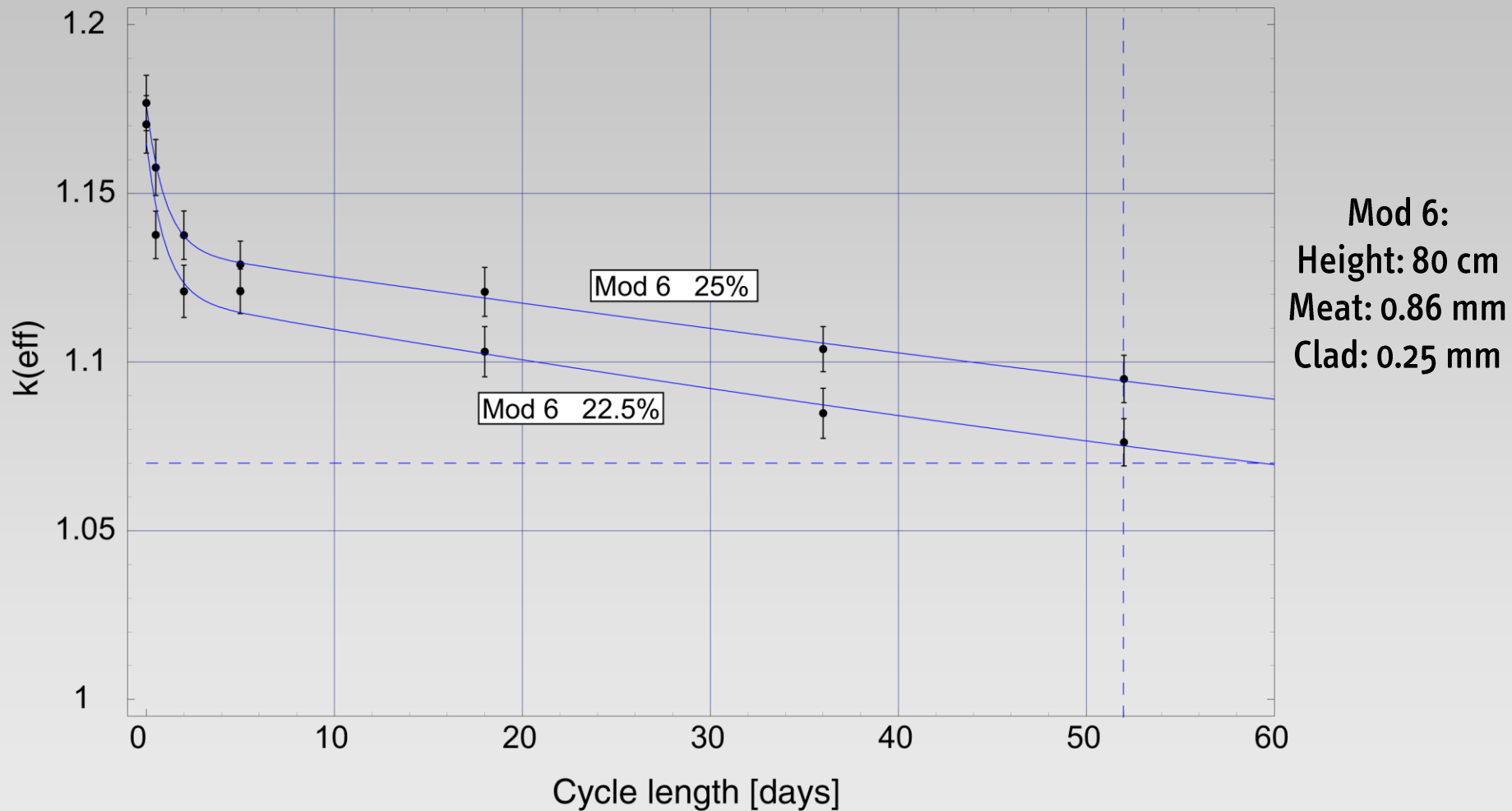


Compensation by Enrichment



	Height	Meat	Clad	Cool	Mass	Enrichment	Plnr.
Mod. 1 Original	70 cm	0.60 mm	0.38 mm	2.20 mm	43.25 kg	32-33 %	113
Mod. 2	80 cm	0.60 mm	0.38 mm	2.20 mm	49.42 kg	26-27 %	113
Mod. 4	70 cm	0.86 mm	0.25 mm	2.20 mm	61.99 kg	27-28 %	113
Mod. 5	70 cm	0.60 mm	0.25 mm	2.46 mm	43.25 kg	27-28 %	113
Mod. 6	80 cm	0.86 mm	0.25 mm	2.20 mm	70.84 kg	24-25 %	113

Cycle Length for Mod 6



Improved strategy (striving for global optimization)

Parameter Space Studies:

simultaneous variations of

x_i : active height, meat cladding and cooling channel thickness

to get $k(\text{eff})_{\text{ini}}(x_i)$ and $\Phi(x_i)$ for LEU fuel

having in mind:

- sufficient initial reactivity, optimum flux,
- keeping constraints like (cycle length, power peaking, heat flux ...)

The parameter study was an intermediate step towards solving the full optimization problem:

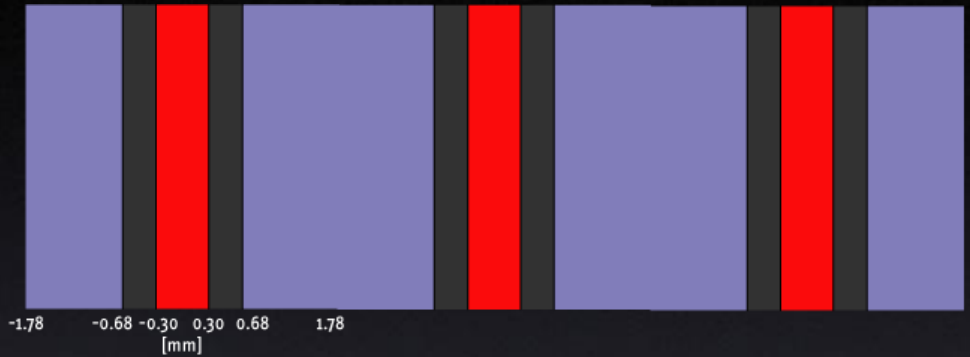
- maximizing reactor performance
- minimizing enrichment (hopefully LEU or near LEU)
- keeping operational constraints

First steps to establish a global optimization routine.

Approach of first investigating a wide range of parameters and then constraining the results

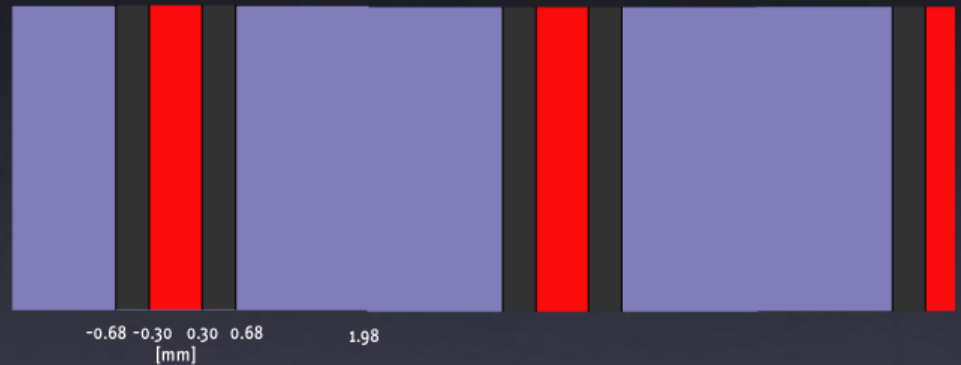
Geometrical Changes II

Varied number of fuel plates

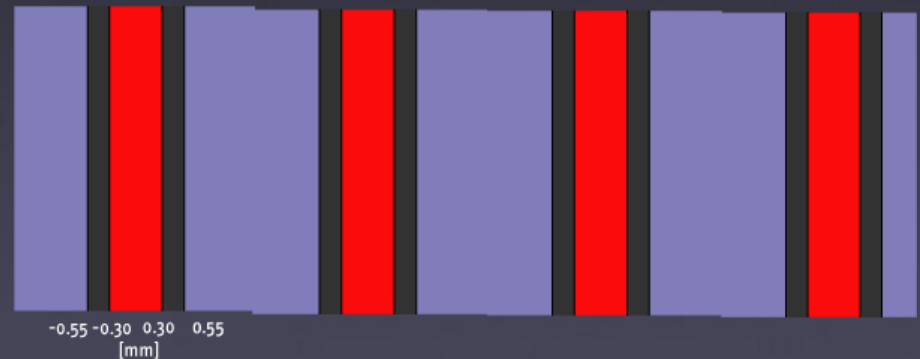


Current Geometry

Wider cooling channels
Less plates

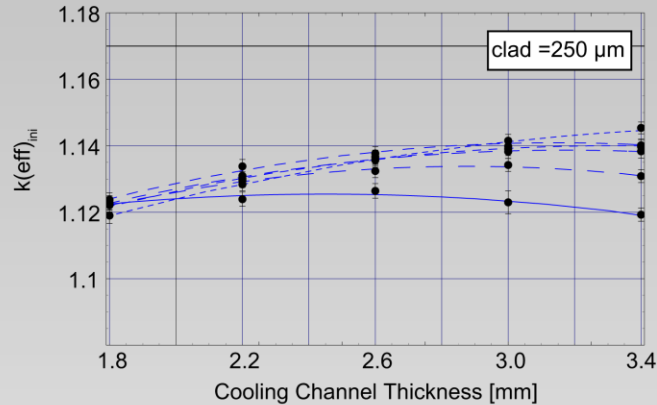
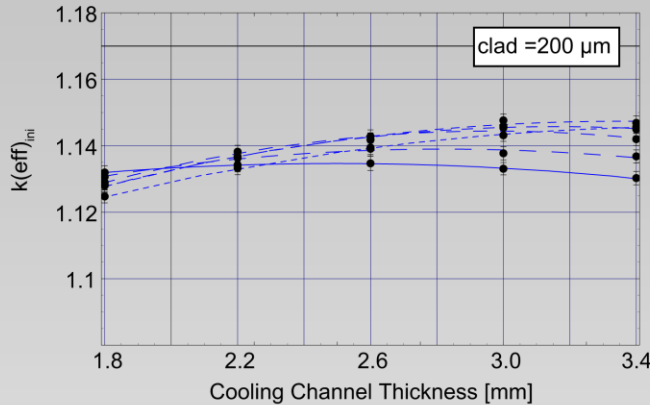


Thinner cooling channels
Thinner clad
More Plates

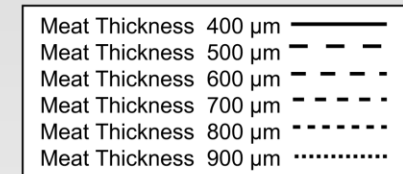
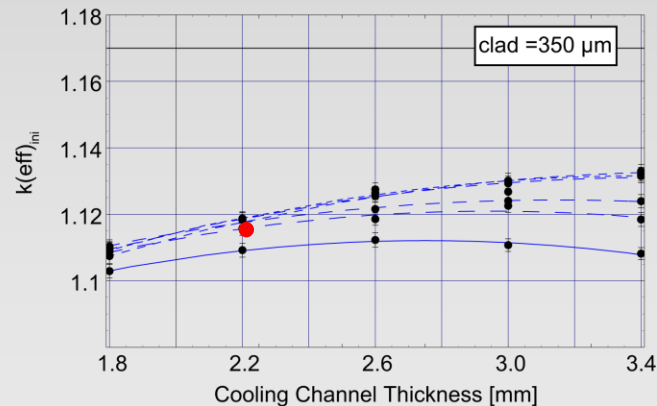
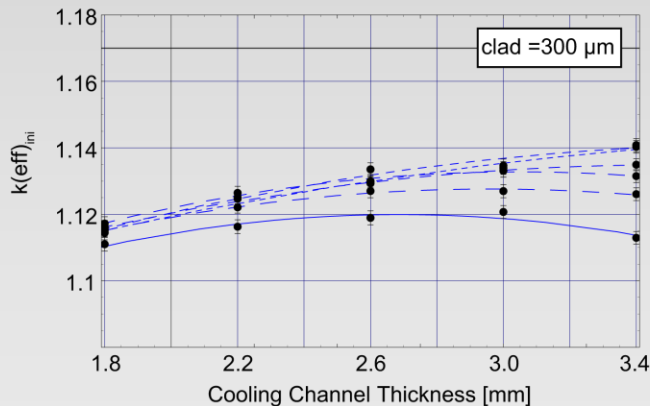


Systematic Study to increase $k(\text{eff})_{\text{initial}}$

Variation of cooling channel, cladding and meat thickness (19.75% enriched, 70 cm)



● Current FRM-II Geometry

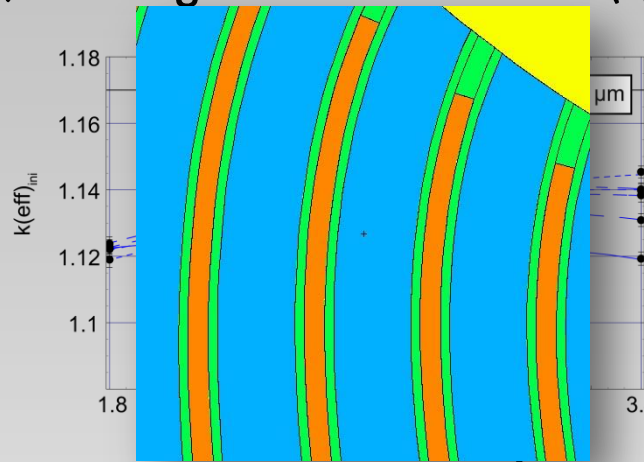
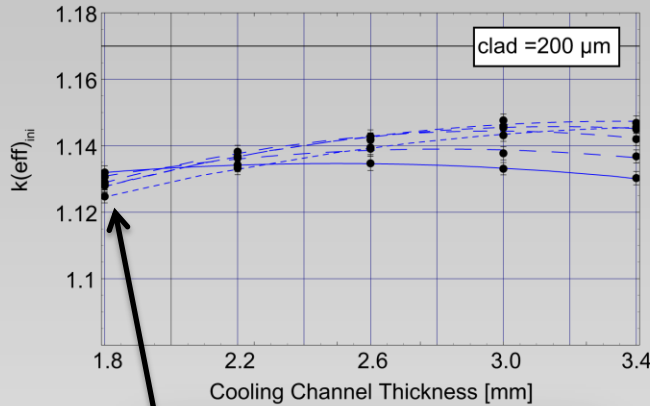


Optimum cooling channel thickness between 2.6 and 3.4 mm

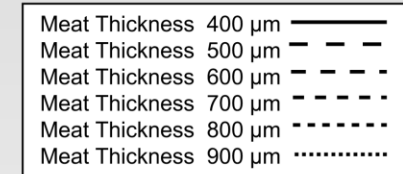
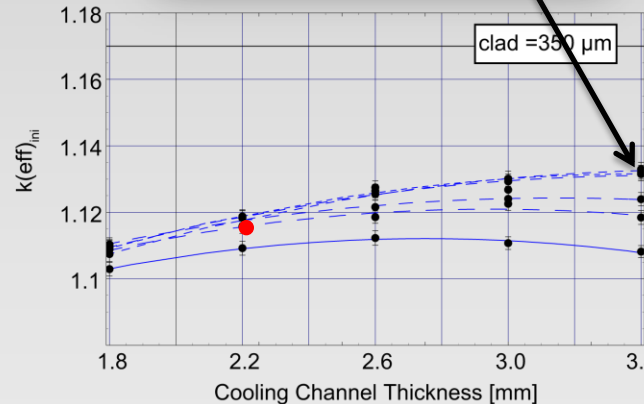
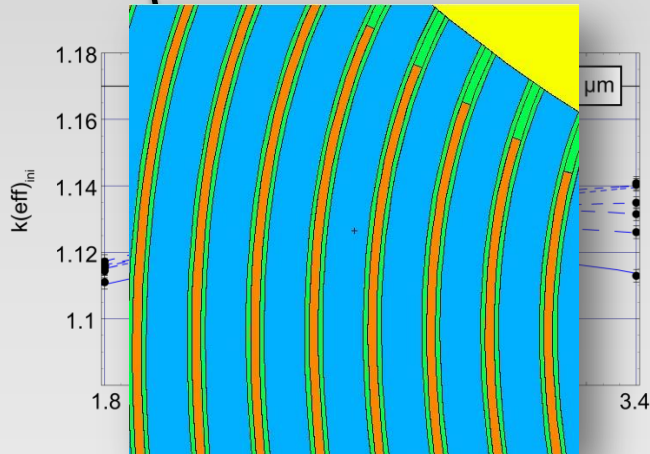
The more cooling channel thickness the more sensitive is $k(\text{eff})$ on the meat thickness

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Variation of cooling channel, cladding and meat thickness (19.75% enriched, 70 cm)



● Current FRM-II Geometry



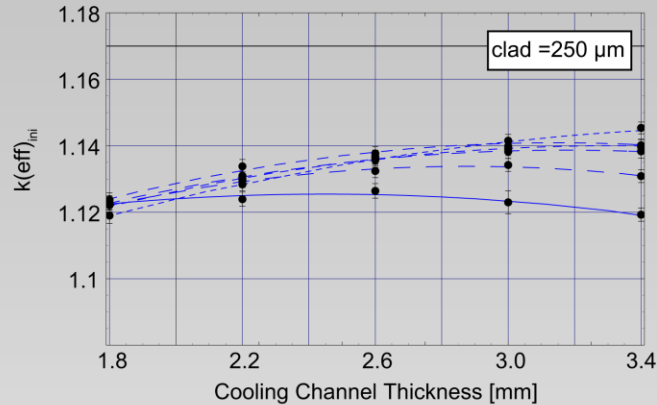
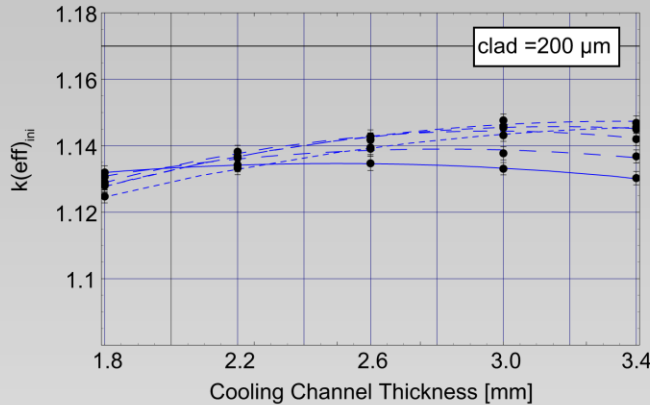
clad = cladding thickness

Optimum cooling channel thickness between 2.6 and 3.4 mm

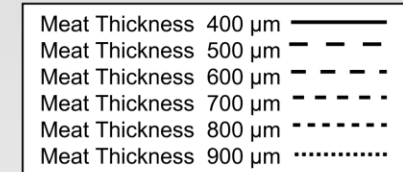
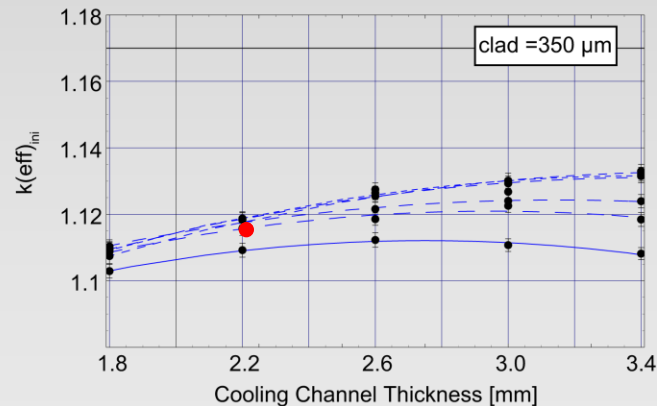
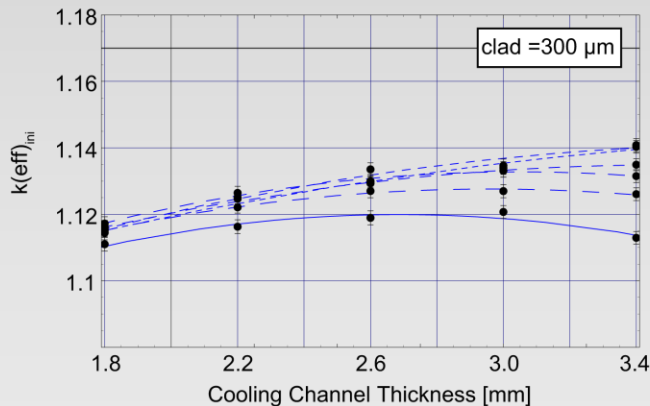
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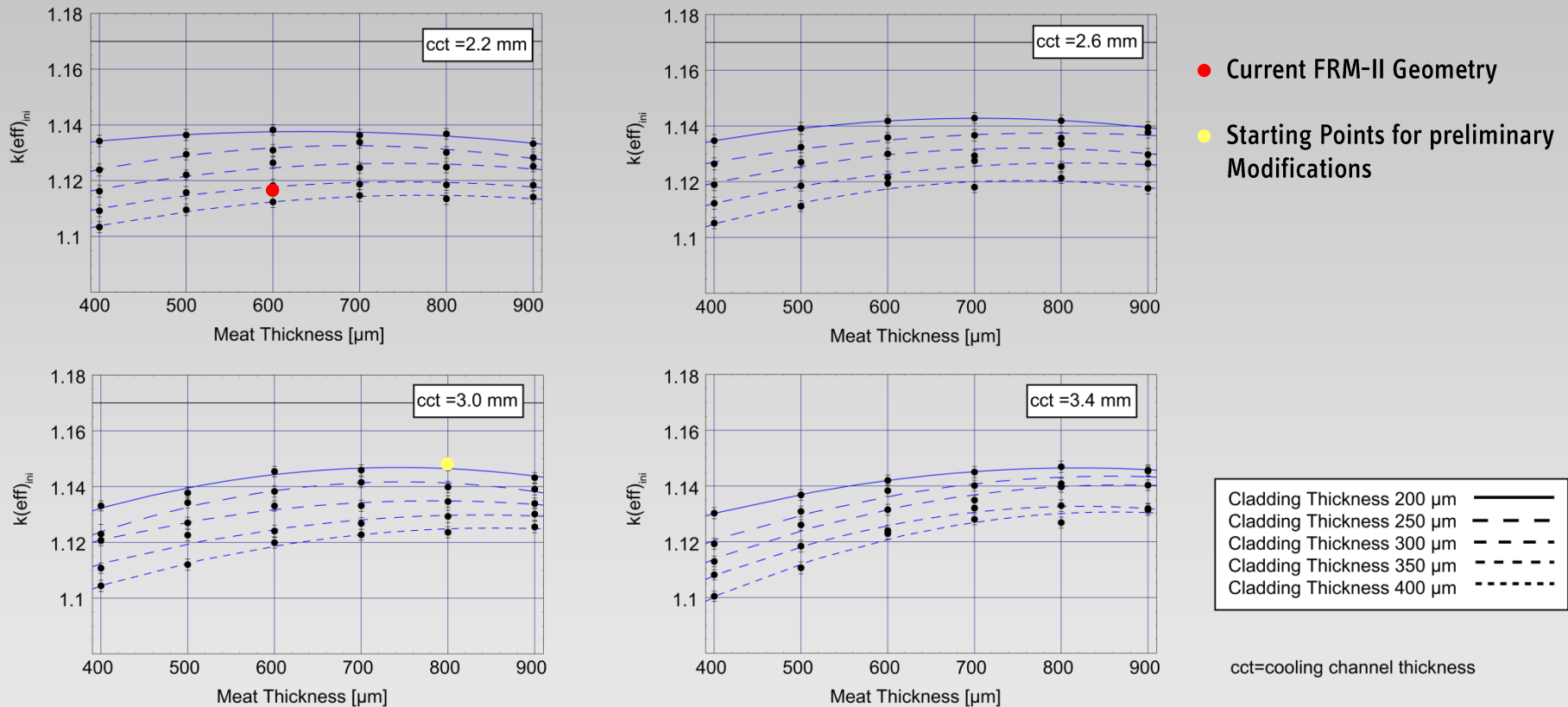


Optimum cooling channel thickness between 2.6 and 3.4 mm

The more cooling channel thickness the more sensitive is $k(\text{eff})$ on the meat thickness

Systematic Study to increase $k(\text{eff})_{\text{initial}}$

Variation of cooling channel, cladding and meat thickness (19.75% enriched, 70 cm)



Optimum meat thickness between 0.7 and 0.9 mm

Lessons from $k(\text{eff})$ study

- Thicker cooling channels with an optimum between $\sim 2.6\text{-}3.4$ mm
- Thin cladding as thin as possible ($\sim < 0.25\text{mm}$)
- Thick meat ($\sim 0.7\text{-}0.9$ mm)
- Reduced number of plates in the core

Two more preliminary modifications based on LEU

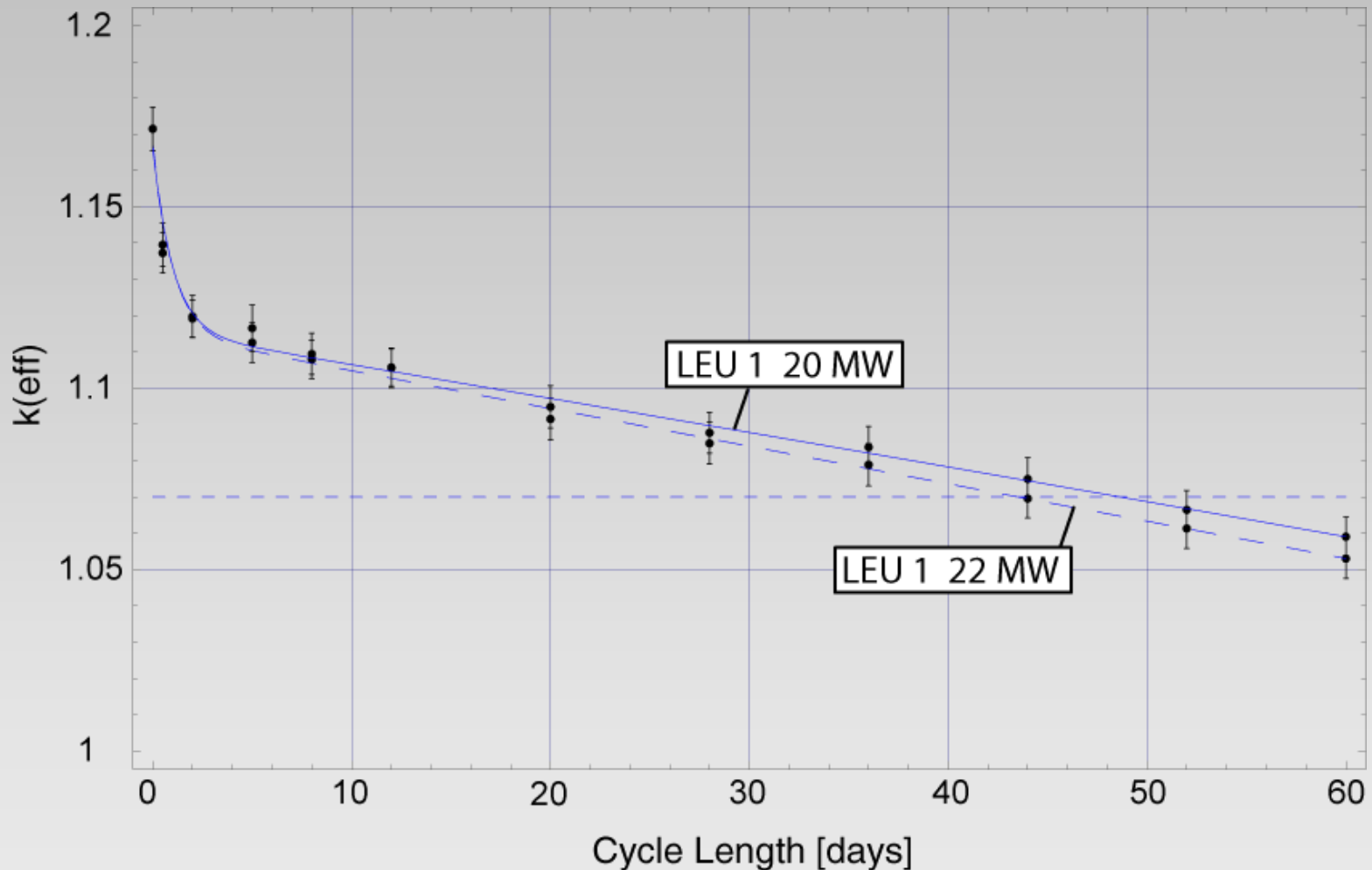
	HEU Design	LEU 1		LEU 2	
Enrichment	93.0%	19.75%		19.75%	
Active Height	70 cm	80cm		84 cm	
Meat	0.60 mm	0.80 mm		0.80 mm	
Cooling Channel	2.20 mm	3.0 mm		3.0 mm	
Cladding	0.38 mm	0.2 mm		0.25	
Power	20 MW	20 MW	22 MW	22 MW	22 MW
Flux loss max	reference	-15.4%	-7.0%	-16.2%	-7.9%
Flux loss CNS	reference	-13.7%	-5.1%	-14.7%	-6.2%
Heat Flux	182 W/cm ²	188 W/cm ²	207 W/cm ²	183 W/cm ²	202 W/cm ²

Unusual thin cladding with 0.2 mm in LEU 1 to investigate potential of very thin cladding.

A candidate for this kind could be Zr-clad plates.

Need to evaluate the minimum thickness for cladding . Of course, this might be interesting for Al-cladding as well.

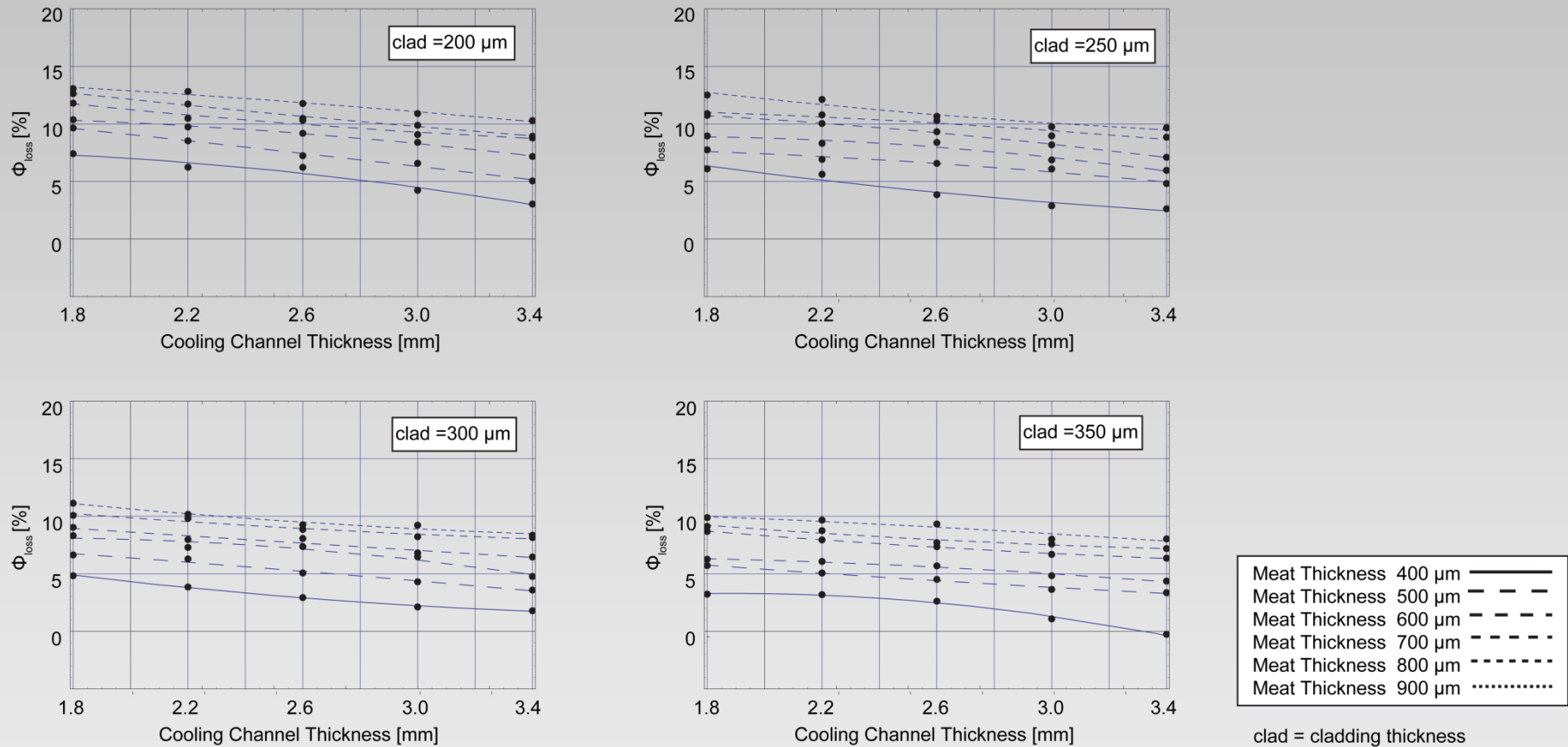
Cycle Length LEU 1



LEU 1 20 MW additional decrease in flux performance of 1-2%
LEU 2 22 MW additional decrease in flux performance of 4-5%

Influence on Flux Losses at Position of Maximum Flux

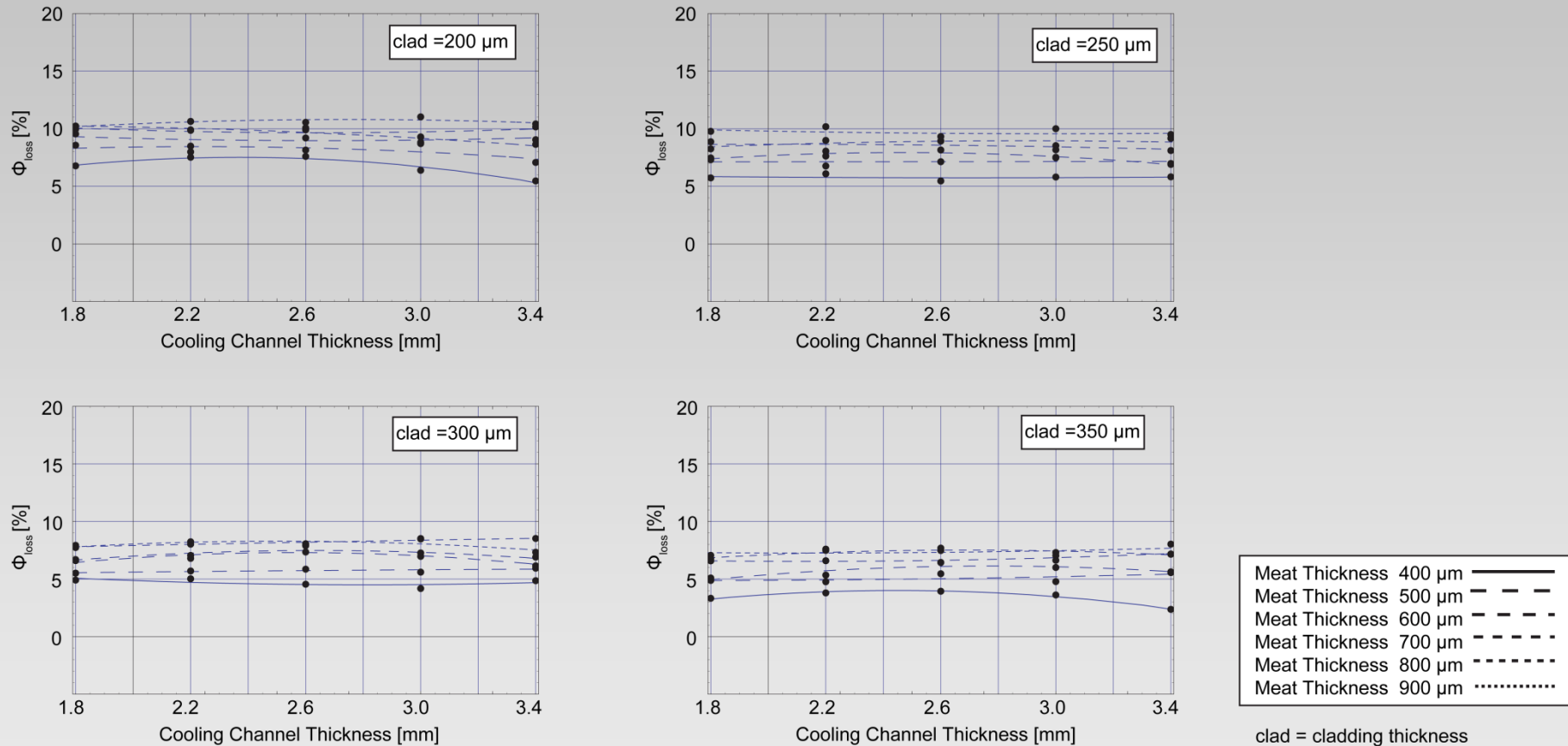
Variation of cooling channel, cladding and meat thickness (19.75% enriched, 70 cm)



Increasing cooling channel thickness reduces flux loss
Reducing cladding thickness increases flux losses
Increasing meat thickness increases flux losses

Influence on Flux Losses at Position of Cold Neutron Source

Variation of cooling channel, cladding and meat thickness (19.75% enriched, 70 cm)

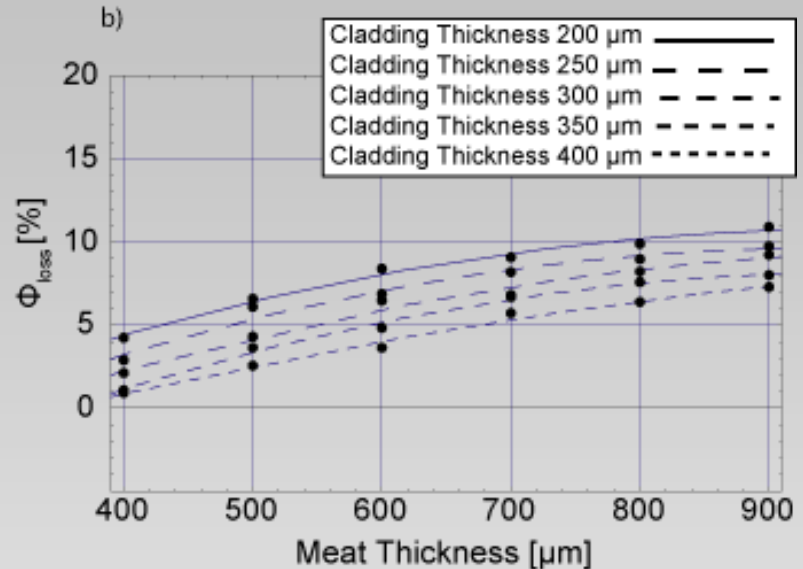
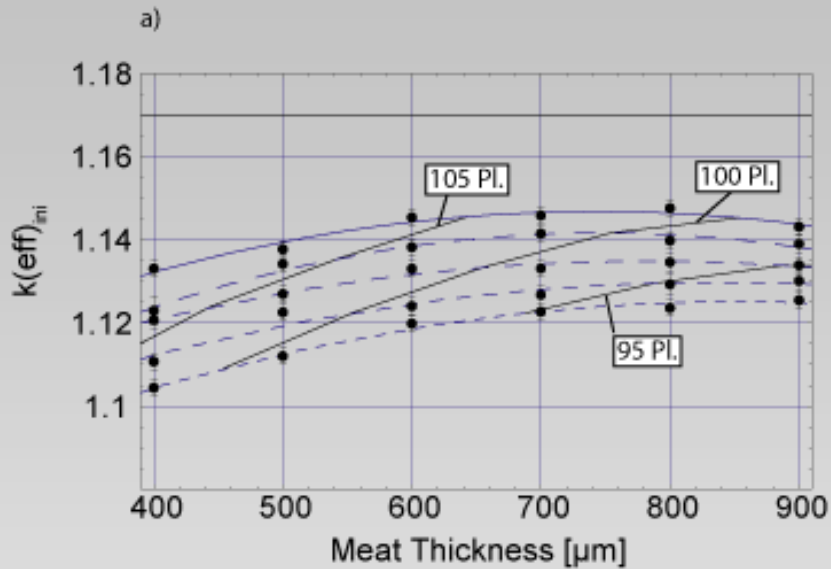


Increasing cooling channel thickness has nearly no influence on flux losses

Reducing cladding thickness increases flux losses

Increasing meat thickness increases flux losses (but less than at max position)

Flux vs $k(\text{eff})_{\text{ini}}$ at Maximum



Cooling Channel thickness 3.0 mm, 70 cm height

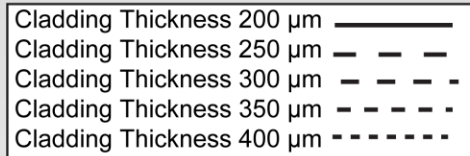
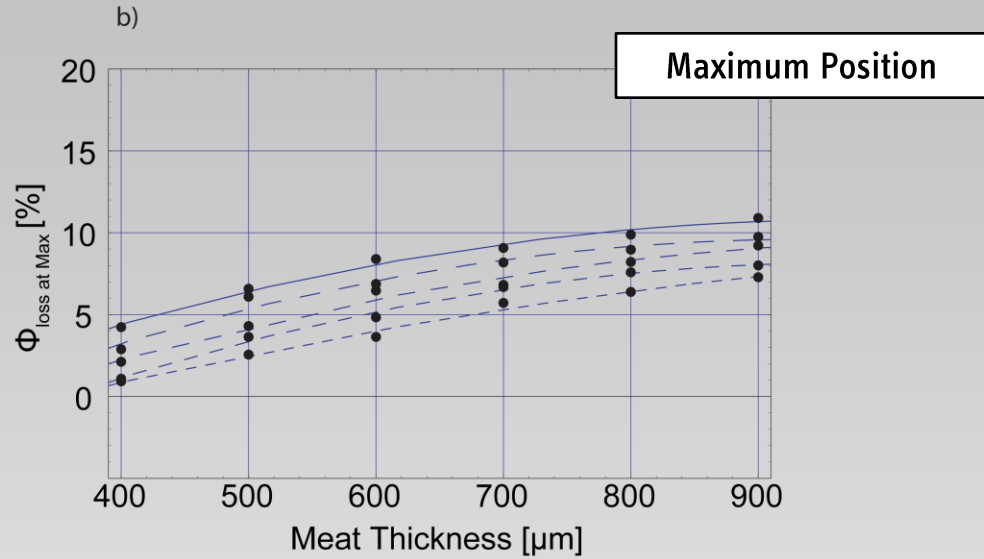
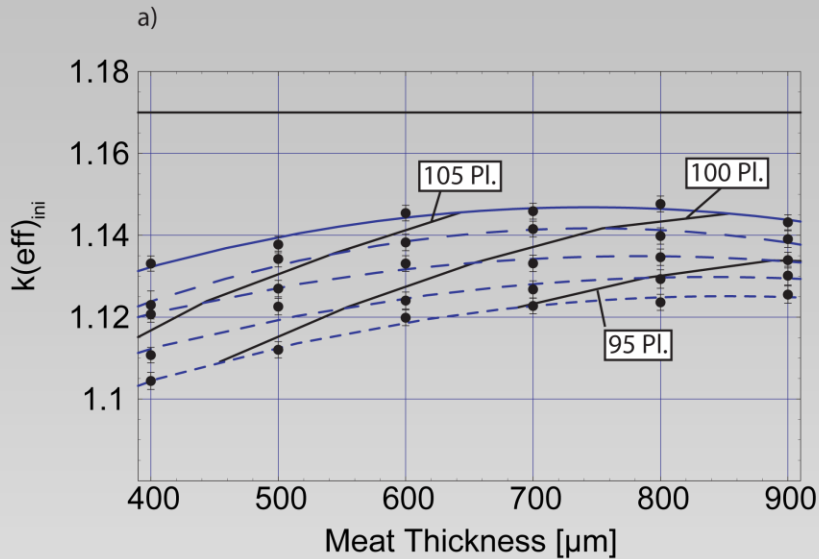
Opposing trends:

Increasing meat thickness to increase $k(\text{eff})_{\text{ini}}$ increases also flux losses

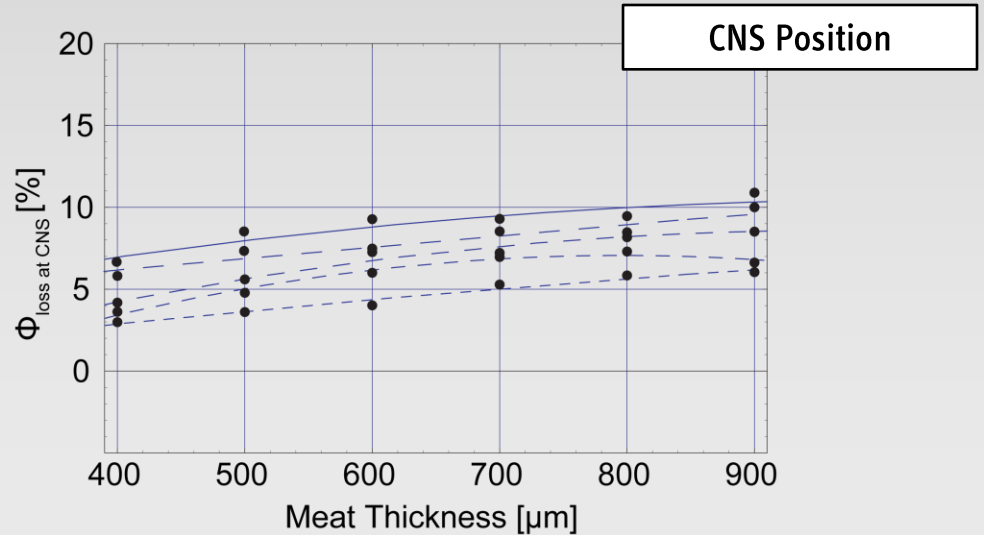
Thinner cladding to increase $k(\text{eff})_{\text{ini}}$ increases also flux losses

-> Need to find optimum

Flux vs $k(\text{eff})_{\text{ini}}$ at CNS



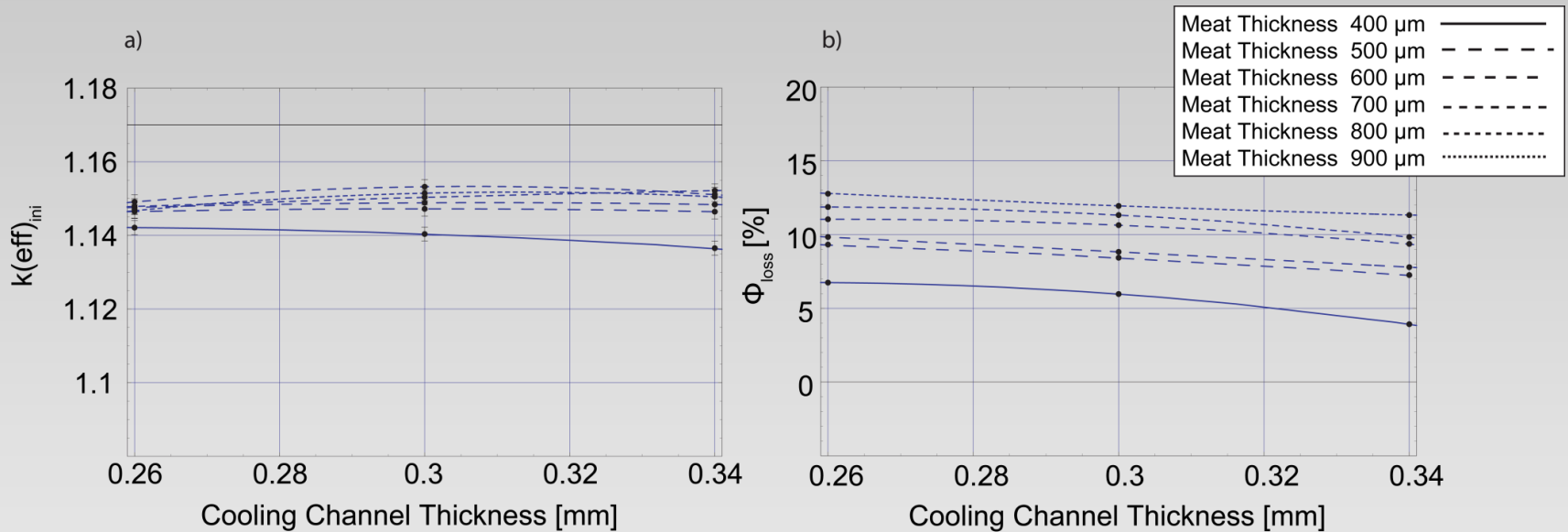
Cooling Channel thickness 3.0 mm



-> Further Investigation of
Flux Profile in Moderator Tank
(with installations and axial profile)

Zr-Cladding

Very thin Zr-Cladding with 150 μm (70 cm height)
Proposed by Argentine Fuel Development Program (E. Pasqualini et al.)



Improving Power density distribution

Radially shaping of meat (axially?)

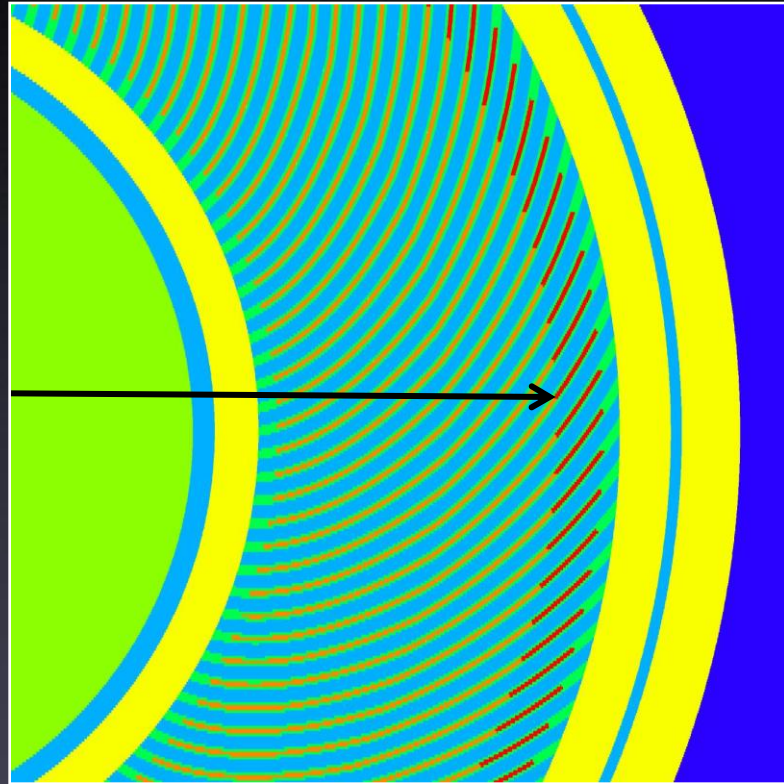
Implementation of stepwise/continuous change of meat thickness into automated inputfile generation

First tentative calculations

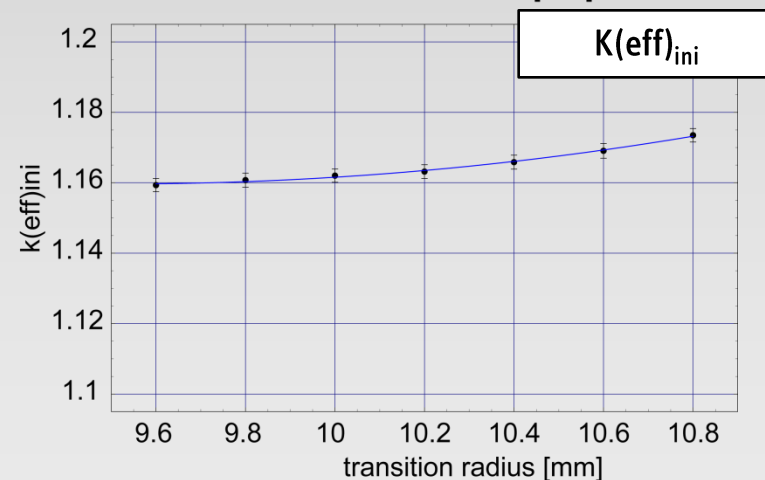
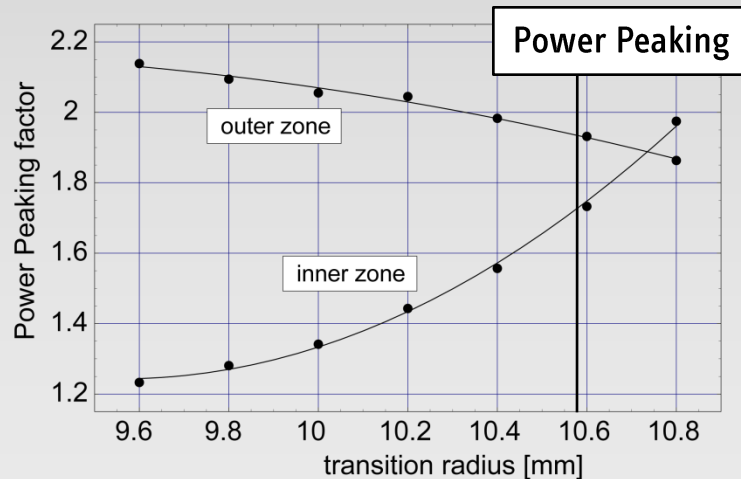
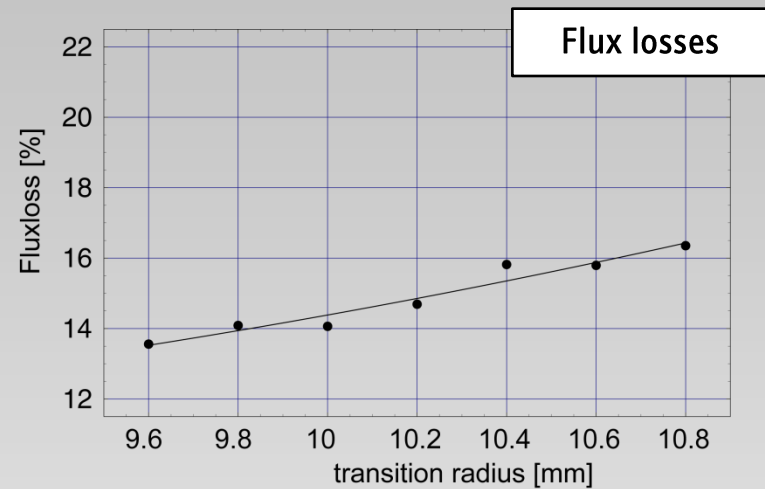
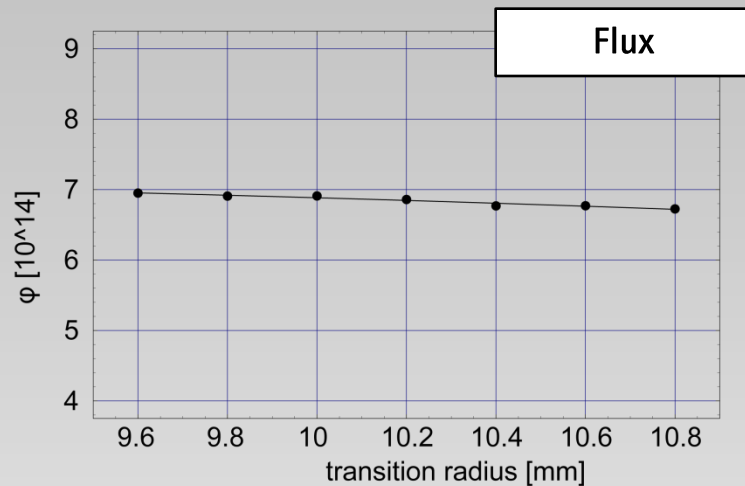
Next step -> finding optimal shape

First Tentative Calculations Changing Transition Radius

Transition Radius
Current Design: 10.59 cm
Variation: 9.6-10.8 cm

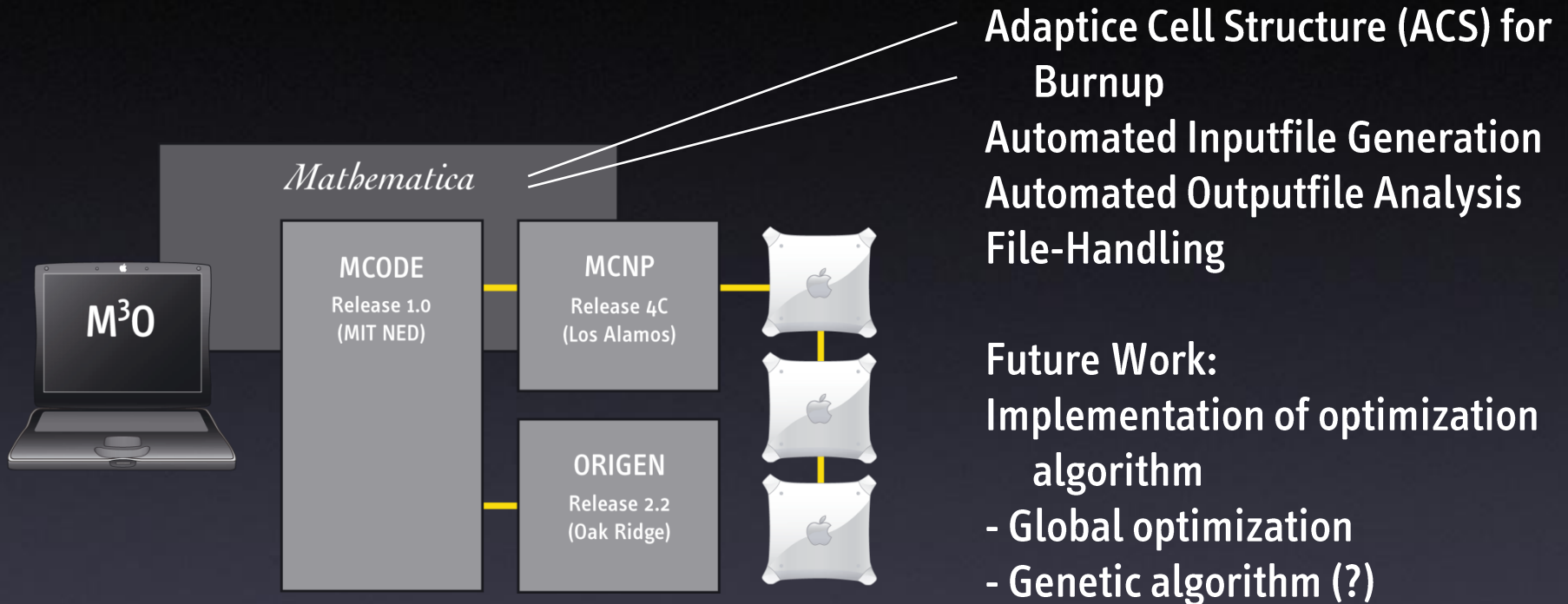


First Tentative Calculations Changing Transition Radius



Based on LEU1 Modification

Computational System

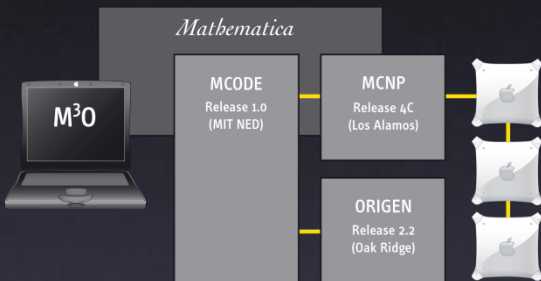


From A. Glaser 2005 or A. Glaser RERTR 2004

-> Need for faster processing of Input decks

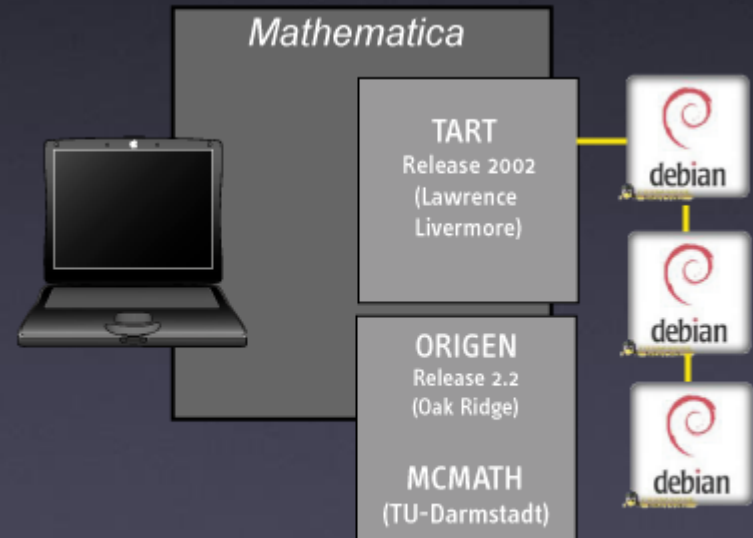
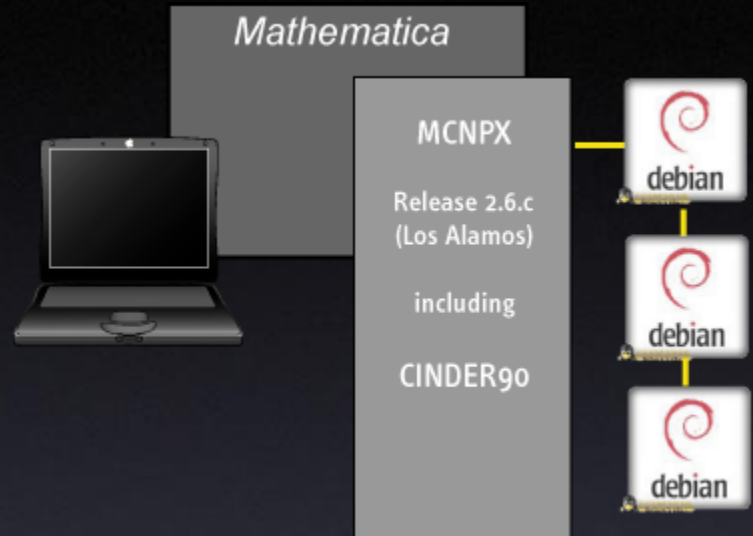
Computational System

Depletion and neutron transport in one code
Faster KCODE than MCNP4c
(multiprocessor)



From A. Glaser 2005 or A. Glaser RERTR 2004

Even Faster KCODE
than MCNPX



Conclusion

For best performing LEU option with UMo monolithic for FRM-II

- cooling channel thickness > 2.2 mm
- increased height to get adequate cycle length
- marginally increased power to improve flux performance
- find optimal trade off between $k(\text{eff})$ and flux depending on variation of meat and cladding thickness

Future Work

- Further steps towards global optimization routine (genetic algorithm?) for high flux one-element research reactors
- Improved reactor model (control rod movement etc.)
- Improved investigation of flux profiles in moderator tank (axial profile) .
- thermohydraulic models and reactivity coefficients
- (Eventually calculations from the source to the experiment by implementing MCSTAS)